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REPORT ON

**HYDROGEOLOGICAL INVESTIGATION
AND TERRAIN EVALUATION
PROPOSED RESIDENTIAL SUBDIVISION
MERRICKVILLE ESTATES
SCOTCH LINE ROAD
TOWNSHIP OF MERRICKVILLE WOLFORD, ONTARIO**

Submitted to:

1605861 Ontario Ltd
(Merrickville Estates)
4273 Green Gables Lane
Gloucester, Ontario
K1V 1S4

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February 2005

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February 28, 2005

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1605861 Ontario Ltd
(Merrickville Estates)
4273 Green Gables Lane
Gloucester, Ontario
K1V 1S4

Attention: Mr. C. Fournier, P. Eng.

RE: HYDROGEOLOGICAL INVESTIGATION AND TERRAIN EVALUATION
PROPOSED RESIDENTIAL SUBDIVISION
MERRICKVILLE ESTATES, SCOTCH LINE ROAD
TOWNSHIP OF MERRICKVILLE-WOLFORD, ONTARIO

Dear Sirs:

This report presents the results of a hydrogeological investigation and terrain evaluation conducted by Morey Houle Chevrier Engineering Ltd. for the above noted proposed residential development.

Should you have any questions on any aspect of this report, or if we may be of further assistance to you on this project, please do not hesitate to contact the undersigned at your earliest convenience.

Yours truly,

Morey Houle Chevrier Engineering Ltd.

C. R. Morey, P. Eng.

File 041-444

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1.0 INTRODUCTION

Morey Houle Chevrier Engineering Ltd. was retained by 1605861 Ontario Ltd. of Gloucester, Ontario to undertake a hydrogeological investigation and terrain evaluation for a site located on Scotch Line Road in the Township of Merrickville Wolford, Ontario (See Key Plan, Figure 1). The development project is known as Merrickville Estates.

The site consists of an area of approximately 100 hectares (270 acres) located on the south/west sides of Scotch Line Road about one kilometer southeast of the Village of Merrickville, in the Township of Merrickville Wolford, Ontario. It is understood that due to the presence of a provincially significant wetland located in the southeast portion of the site only about two thirds of the site, or about 67 hectares, will be developed for residential purposes. The present development plan is to subdivide that portion of the site into some 67 lots for single family dwelling construction. The proposed dwellings will be serviced by private septic systems and wells. The minimum lot size will be 0.8 hectares with the average lot size in excess of 1.0 hectare. Local residential roadways will be constructed to service the lots.

The site is bordered on the north by some scattered residential development, undeveloped land development and the Village of Merrickville beyond. A former land fill, closed some 20 to 25 years ago, exists about 400 metres north of the site. All of the dwellings near the site are serviced by private septic systems and wells. Undeveloped land and wetlands/low lying areas exist on the east, south and west sides.

Based on a review of the surficial geology map for the site area, it is expected that the portion of the site to be developed is underlain for the most part by a thin veneer of sandy overburden follow by bedrock consisting of dolomite of the Oxford formation. Some fine to medium sand deposits may be present in the northwest portion of the site.

A report entitled Village of Merrickville -Wolford Municipal Groundwater Management Study, prepared by Golder Associates Ltd. in 2000, includes the present study area. That report indicates that the groundwater flow for the aquifer intercepted by the Village of Merrickville wells is from south to north towards the Rideau River. The report indicates that the average precipitation for the area is 910 millimetres, with normal annual potential evapotranspiration of 547 millimetres and normal annual water surplus of 364 millimetres. The report indicates that most of the Village of Merrickville-Wolford is a transitional zone with regards to groundwater discharge/recharge. The report indicates that the proposed subdivision is within a "Restricted Use Zone" from a municipal well head protection point of view. The County of Leeds Grenville has

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confirmed that there are no known or documented environmental constraints to residential development on private on-site services on or in the area of the subject lands.

2.0 FIELD PROCEDURES

The objectives of this study were:

- * to determine the shallow subsurface soil and groundwater conditions relative to the design of Class IV septic sewage disposal systems.
- * to investigate the potential quantity and quality of groundwater available from drilled wells for domestic supply.
- * to investigate any inter connectivity between the supply aquifer and the receiving aquifer.

2.1 Terrain Evaluation

The field work for the terrain evaluation was carried out on November 4, 2004 at which time sixteen test pits were put down across the site. The test pits were advanced to depths of some 0.2 to 2.3 metres below the existing ground surface using a tire mounted back hoe supplied and operated by a local excavating contractor. The soils types, depths to strata changes, and groundwater conditions were recorded at each test pit location by a member of our engineering staff. Monitoring wells were installed in test pits 6, 10 and 16 and two additional monitoring wells with installations, number MW 2-1/2-2 and MW 3-1/3-2 were drilled into the upper bedrock for the purpose of sampling and testing for nitrate and to determine the upper groundwater flow direction. A sample of groundwater was obtained from each of the monitoring wells and submitted to Accutest Laboratories for nitrate testing on February 22, 2005.

The approximate locations of the test pits and monitoring wells are shown on the attached Site Plan, Figure 2 and a description of the various soils and groundwater conditions encountered in the test pits is given in the attached Table I.

2.2 Groundwater Supply Investigation

To determine the quantity and quality of groundwater available for domestic water supply, six test wells numbered TW 1, TW 2, TW 3, TW 4, TW 5 and TW 6 were pump tested and sampled. The approximate locations of the test wells are shown on the attached Site Plan, Figure 2, as symbols W1 to W6, respectively. Test wells TW 1 and TW 2 were drilled on December 14, 2004, TW 3 on November 29, 2004, and TW 5 and TW 6 on January 31, 2005 by Air-Rock Drilling Co. Ltd. of Richmond, Ontario. (see Appendix C).

The water well records for the test wells supplied by the well drillers indicate that nominal 16 centimetre inside diameter steel casings were installed through the overburden and were set well into the bedrock and grouted in place. The wells were drilled to final depths using a 15 centimetre diameter bit and completed as an open hole in the bedrock. TW 1, TW 2, TW 3, TW 4, TW 5 and TW 6 were drilled into the bedrock to final depths of some 36.6, 30.5, 30.5, 30.5, 24.4 and 24.4 metres, respectively, below the existing ground surface.

Pumping tests were conducted on TW 2 and TW 3 on December 29 and December 9, 2004, respectively and on TW 1, TW 4, TW 5 and TW 6 on January 9, February 11, February 7 and February 8, 2005, respectively. The pumping tests consisted of a 6 to 10.5 hour duration constant discharge rate pumping test. During the pumping tests, water level measurements were made on a regular basis to monitor the drawdown of the water level in the wells in response to pumping. After the pumping period, the pump was shut off and the recovery of the water level in the test wells was monitored for a period of time.

Groundwater samples were collected from the test wells at about hour 1 or 3 and at hour 6 of the pump tests to characterize groundwater quality. The groundwater samples from the test wells were collected and prepared/preserved in the field using appropriate techniques and submitted to Accutest Laboratories Ltd. in Nepean, Ontario for the chemical, physical and bacteriological analyses listed in the Ministry of the Environment (MOE) guideline entitled Procedure D-5-5, Technical Guideline for Private Wells: Water Supply Assessment, August 1996. The temperature, conductivity, pH, turbidity, sulphide and residual chlorine levels of the groundwater were measured at periodic intervals during the pumping tests.

3.0 TERRAIN EVALUATION

3.1 Soil and Groundwater Conditions

This section provides a summarized account of the subsurface soil and groundwater conditions on the subject property based on the information obtained at the test pit locations. Details of the subsurface conditions at each test hole location are presented in the attached Table I. It is noted that in some cases the stratigraphic boundaries within the overburden represent a transition between soil types rather than an exact plane of geologic change. Subsurface conditions differing somewhat from those reported can be expected to exist at the site.

In general, the overburden materials at the site are indicated to consist of topsoil followed by bedrock or topsoil overlying a relatively thin layer of sand or silty sand followed by bedrock.

Topsoil was encountered from the surface at all of the test pit locations except test pit 16. The topsoil typically ranges in thickness from some 0.2 to 0.3 metres. Beneath the topsoil, at most of the test pits a deposit of red brown to yellow brown to grey brown sand to silty sand was encountered ranging in thickness from about 0.2 to 2.0 metres. Test pit 16 encountered sand fill from the surface and was terminated in the native sand material at a depth of some 2.1 metres below the existing ground surface. Bedrock was encountered beneath the topsoil or sand/silty sand, at all of the remaining test pits.

All of the test pits were dry upon completion of excavating on November 4, 2004.

The total overburden thickness, as indicated by the test well records provided by the well driller and the results of the test pits ranges from about 0.2 to 2.3 metres.

3.2 Class IV Septic Sewage Disposal Systems

This section discusses the implications of the site-specific terrain conditions in terms of the feasibility of installing Class IV septic sewage disposal systems on the proposed lots.

3.2.1 Septic System Envelopes

The septic system envelope area (septic envelope) represents the area on a lot set aside for the construction of the leaching bed and is for the leaching bed only and does not include that area required for the septic tank or the isolation/separation distances required by the Ontario Building Code. The deposit or disposal of any materials or the placement of any structure or the operation of any equipment, other than material, structures or equipment required for the construction of the sewage system within or upon the septic envelope is prohibited.

The size of the septic envelopes are a function of the percolation time of the native soil in the vicinity of the septic envelope or the fill used for construction of a septic bed and the daily effluent loading to the septic bed. The percolation rate for the sand and silty sand soils at this site is estimated at between 5 and 20 minutes per centimeter.

As a conservative approach to determining the expected largest septic system envelope required to service a single family dwelling at this site, a septic system envelope size was calculated assuming a fully raised bed using a percolation rate of 8 minutes per centimetre for the imported sand required and a daily sewage flow of 3000 litres. A design flow of 3000 litres per day is suitable for a five bedroom dwelling with 250 square metres of finished area and 30 fixture units. For comparison purposes, the septic system envelope for a more traditional size dwelling having a daily effluent design flow of 2000 litres per day was also calculated. The following formulae were used to calculate the size of the septic envelope:

The larger of

$$A = Q/6$$

or

$$A = 1.6 QT/200$$

plus

4:1 Leaching Bed Side Slopes and
Typical Mantle Area of 15 x 15 metres

where Q = daily sewage flow for the proposed dwelling (i.e., 3,000 litres per day)

T = percolation rate of imported fill material

The required size of the septic envelopes, based on the approach described above, is approximately 700 square metres (design flow 3000 l/d) and 550 square metres (design flow 2000 l/d). Given the proposed lot areas, sewage servicing using septic systems is considered acceptable.

Prior to establishing the actual septic envelope (leaching bed) location on any particular lot, several test holes should be excavated to determine the consistency/variability of the overburden in the vicinity of the proposed septic envelope and percolation rate tests should be carried out to determine the actual envelope area required. Where possible, the septic envelope on the proposed lots should be located in an area with the greatest thickness of native soil. Where less than about a 300 millimetre thickness of native soil will exist over the bedrock in a septic envelope area, it may be necessary to provide a suitable thickness of relatively impermeable material such as silty clay throughout the septic envelope to prevent direct entry of septic effluent into the bedrock.

Other site-specific considerations with respect to the locations of the septic envelopes (leaching beds) on the proposed lots are as follows:

- * assuming that shallow groundwater flow within the upper overburden is from topographically higher areas to topographically lower areas, the septic envelopes should be situated in the topographically lower areas with the wells in the topographically higher areas.
- * the separation distances between leaching beds and properly constructed drilled wells should be at least 15 metres for any inground beds and up to 18 metres for fully raised beds as required under the Ontario Building Code.
- * in view of the shallow bedrock conditions throughout most of the site it is considered that Ontario Building Code approved tertiary treatment systems should be incorporated in the design of all the septic systems for the proposed development.

3.2.2 Leaching Bed Design Considerations

The design of leaching beds is a combination of a number of interrelated factors including effluent discharge volume, properties of the soil materials in the leaching bed, length of distribution lines and the subsurface conditions. The construction of individual septic disposal systems on the proposed lots should be carried out in accordance with the specifications set out in the Ontario Building Code.

The design must ensure that the bottom of the absorption trenches is at least 0.9 metres above bedrock or soils which are unsuitable for treatment of septic effluent (those with excessively low permeability), and at least 0.9 metres above the seasonally high groundwater table.

Based on the soil and groundwater conditions at the site, partially to fully raised type septic system leaching beds are likely to be used. In view of the variable subsurface conditions encountered in the test pits which range from sand to silty sand to bedrock, the actual leaching bed type appropriate for each lot will depend on the individual lot specific soil, bedrock and groundwater conditions.

Any partially to fully raised leaching beds should be constructed of imported sand having a percolation time of between 4 and 8 minutes per centimetre. It is recommended that in situ percolation rate tests and/or gradation analyses be carried out on any potential sand fill prior to leaching bed construction in order to verify that the percolation time of the fill material is acceptable.

Current regulations require that the upper 0.25 metre thickness of soil (soil mantle) underlying the raised portion of the leaching bed and extending at least 15 metres beyond the outer distribution pipes in any direction that effluent may migrate, has a percolation time between 1 and 50 minutes per centimetre. Although the native sandy soil in some portions of the site likely conforms to the desired percolation time for the purpose of constructing the soil mantle, the overburden in the downgradient directions from the leaching bed should be investigated on a lot-specific basis to ensure that the 0.25 metre depth requirement is met. If necessary, suitable imported fill may be used to construct the mantle or to augment the natural soil. It is suggested that the native soils be left in place when the leaching beds are constructed.

3.3 Groundwater Impact Assessment

The results of the test pits put down at the site for the terrain evaluation described above indicate that the aquifer receiving effluent from the proposed on site septic systems is for the most part the upper overburden consisting of sand and silty sand. Some areas of relatively shallow bedrock were encountered at the test pits and accordingly, for a portion of the site, the receiving aquifer may consist of the upper bedrock

To obtain a general indication as to the potential impact of septic effluent on the properties adjoining the proposed subdivision, a nitrate dilution model was utilized. Information from the Ministry of the Environment indicates that for sandy soils and fractured bedrock a water surplus of 372 millimetres per year

and 460 millimetres per year, respectively, may be used for the Ottawa area. In addition the previously mentioned Village of Merrickville-Wolford Municipal Groundwater Study indicates an annual surplus of 364 millimetres. A daily effluent loading of 1000 litres per day per septic system was assumed. A maximum nitrate level of 1.27 milligrams per litre was measured in the receiving aquifer at the overburden and upper bedrock monitoring wells. That nitrate level was used as the background nitrate level for the impact dilution calculation.

With regard to treatment and dispersal of effluent from the leaching beds, the expected impact of septic systems at this site was determined by considering the attenuation of nitrate in the effluent from an assumed 40 milligrams per litre (mg/l) (as N) at the septic tanks to 10 mg/l (as N) at the property boundary by dilution as a result of the infiltration of meteoric water only. The results of the calculations indicate that the expected concentration of nitrate at the site boundaries due to 67 septic systems including the maximum measured nitrate background level is about 4.7 milligrams per litre which is well within the Ministry of the Environment acceptable nitrate impact limit of 10 milligrams per litre (See Appendix G).

Based on the impact assessment, the development of the site on private sewage disposal systems is not expected to have an adverse impact on groundwater resources in the site area.

4.0 GROUNDWATER SUPPLY INVESTIGATION

4.1 Supply Aquifer

As mentioned above, bedrock geology maps indicate that the site is underlain by dolomite of the Oxford formation. A review of the attached MOE water well records for the test wells supplied by the well drillers indicate water was found during drilling in grey limestone at depths of some 19 to 34 metres.

4.2 Water Quality

The results of the chemical, physical and bacteriological analyses of water samples from the test wells are provided in the attached Appendix B and in Table I. The water meets all the Ontario Drinking Water Standards (ODWS) health and aesthetic parameters tested for at the wells except for the following,

- turbidity and hardness at all of the wells

- iron at TW 1, TW 2, TW 4 and TW 5
- hydrogen sulphide at TW 3
- total organic nitrogen at TW 4
- total coliform at TW 5

The turbidity levels in the water samples from the test wells measured at the laboratory ranged from 0.2 to 19.5 NTU compared to the Ontario Drinking Water Standard (ODWS) of 1 NTU. It is expected that the turbidity levels measured at the laboratory reflect the precipitation of iron in the samples between the time sampled and tested in the laboratory. Well head turbidity testing carried out during the pump tests gave values for turbidity of less than 1 NTU at all of the test wells.

The water sample obtained from TW 5 contained one total coliform for the 6 hour sample and 0 total coliform for the 3 hour sample. The presence of total coliform in a newly drilled well is common. It is considered that TW 5 could be adequately disinfected by chlorination.

The level of hydrogen sulphide measured in the water sample from TW 4 and the levels of iron measured in the water samples from test wells TW 1, TW 2, TW 4 and TW 5 were above the ODWS but are well within the MOE treatability limit using water softeners or manganese greensand filters. The water samples from all the test wells are considered to be somewhat hard by water treatment standards. Water with a hardness above 80 to 100 milligrams per litre as CaCO_3 is often softened for domestic use. Water softening by conventional sodium ion exchange may introduce undesirably high concentrations of sodium into the drinking water. Where ion exchange water softeners are used, a separate unsoftened water supply could be used for drinking and culinary purposes.

The level of organic nitrogen measured at TW 4 was 0.07 milligrams per litre at hour 3 and 0.27 milligrams per litre at hour 6 compared to the ODWS of 0.15 milligrams per litre. Total organic nitrogen measured above the ODWS can possibly indicate a source of surface contamination. However, as the results of the bacteriological testing, which is a more positive indicator of surface source contamination, indicated no bacteriological contamination in either the 3 hour sample or the 6 hour sample, it is considered that the measured organic nitrogen level measured at TW 4 is of no health related concern.

The level of sodium measured at TW 3 was slightly above 20 milligrams per litre (21 milligrams per litre) and accordingly may be of interest to persons on a sodium restricted diet. The sodium levels measured may

be of interest to the local Medical Officer of Health to be passed on to local physicians for their use with patients on sodium restricted diets.

A sample of water from the well servicing the existing dwelling at 173 Collar Hill Road located in close proximity of the northeast corner of the site was obtained and delivered to Accutest Laboratories Ltd for testing for the Subdivision Package list of parameters. The results of that testing are provided in the attached Appendix K and indicated that the sample meets all of the ODWS tested for except hardness which is well within the MOE treatability limits.

4.3 Water Quantity

The drawdown and recovery data and plots for the test wells are shown in Appendices D, E, F, G, H and I. The drawdown and recovery data provided were measured with reference to the top of the well casing at each test well location.

The pumping test data for the test wells were analyzed using the method of Cooper and Jacob (1946). Although the assumptions on which these equations are based are not strictly met, this method provides a reasonable estimate of the aquifer transmissivity.

The following sections discuss the results of the analysis of the data obtained during the pumping tests with respect to the test well yield.

4.3.1 Test Well TW 1

The 7.5 hour duration pumping test was conducted at a discharge rate of about 112 litres per minute (25 lpm). The static water level prior to pumping was 2.63 metres below the top of the well casing and the water level after 7.5 hours of pumping was 5.87 metres below the top of the well casing for a total drawdown at the end of pumping of 3.24 metres. The available drawdown in the well is about 32.5 metres. The specific capacity of the well at this pumping rate is approximately 50 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is calculated to be 250.1 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 200.1 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 225.1 m²/day.

At the end of pumping, it required 25 minutes for 95 percent recovery of the total drawdown in the static water level created during pumping.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 112 litres per minute (25 Igpm), and that during the course of the 7.5 hour pumping period only about 10 percent of the available drawdown in the test well was utilized.

4.3.2 Test Well TW 2

The 10.5 hour duration pumping test was conducted at a discharge rate of about 79 litres per minute (17 Igpm). The static water level prior to pumping was 0.2 metres below the top of the well casing and the water level after 10.5 hours of pumping was 12.83 metres below the top of the well casing for a total drawdown at the end of pumping of 12.63 metres. The available drawdown in the well is about 28.8 metres. The specific capacity of the well at this pumping rate is approximately 9 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is calculated to be 43.2 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 1.8 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 22.5 m²/day. At the end of pumping, it required 18 minutes for 99 percent recovery of the total drawdown in the static water level created during pumping.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 79 litres per minute (17 Igpm), and that during the course of the six hour pumping period only about 44 percent of the available drawdown in the test well was utilized.

4.3.3 Test Well TW 3

The 8 hour duration pumping test was conducted at a discharge rate of about 102 litres per minute (22 Igpm). The static water level prior to pumping was 2.65 metres below the top of the well casing and the water level after 8 hours of pumping was 2.83 metres below the top of the well casing for a total drawdown at the end of pumping of 0.18 metres. The available drawdown in the well is about 26.4 metres. The specific capacity of the well at this pumping rate is approximately 817 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is calculated to be 375.2 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 150.0 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 262.3 m²/day. At the end of pumping, it required 54 minutes for 83 percent recovery of the total drawdown in the static water level created during pumping.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 102 litres per minute (22 Igpm), and that during the course of the 8 hour pumping period only about 1 percent of the available drawdown in the test well was utilized.

4.3.4 Test Well TW 4

The six hour duration pumping test was conducted at a discharge rate of about 114 litres per minute (25 Igpm). The static water level prior to pumping was 5.19 metres below the top of the well casing and the water level after six hours of pumping was 5.72 metres below the top of the well casing for a total drawdown at the end of pumping of 0.53 metres. The available drawdown in the well is about 23.8 metres. The specific capacity of the well at this pumping rate is approximately 309 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is calculated to be 142.9 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 200.1 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 171.5 m²/day. At the end of pumping, it required 30 minutes for 89 percent recovery of the total drawdown in the static water level created during pumping.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 114 litres per minute (25 Igpm), and that during the course of the six hour pumping period only about 2 percent of the available drawdown in the test well was utilized.

4.3.5 Test Well TW 5

The six hour duration pumping test was conducted at a discharge rate of about 114 litres per minute

(25 l/gpm). The static water level prior to pumping was 4.45 metres below the top of the well casing and the water level after six hours of pumping was 4.73 metres below the top of the well casing for a total drawdown at the end of pumping of 0.28 metres. The available drawdown in the well is about 18.5 metres.

The specific capacity of the well at this pumping rate is approximately 586 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is estimated to be 500.3 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 300.2 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 400.2 m²/day. At the end of pumping, it required 18 minutes for 61 percent recovery of the total drawdown in the static water level created during pumping. The well recovered to 96 percent of the total drawdown in 965 minutes.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 114 litres per minute (25 l/gpm), and that during the course of the six hour pumping period only about 2 percent of the available drawdown in the test well was utilized.

4.3.6 Test Well TW 6

The six hour duration pumping test was conducted at a discharge rate of about 65 litres per minute (14 l/gpm). The static water level prior to pumping was 5.93 metres below the top of the well casing and the water level after six hours of pumping was 19.46 metres below the top of the well casing for a total drawdown at the end of pumping of 13.53 metres. The available drawdown in the well is about 17.0 metres. The specific capacity of the well at this pumping rate is approximately 7 cubic metres per day per metre of drawdown.

Based on the pumping test drawdown data the transmissivity of the aquifer is calculated to be 8.6 m²/day. Based on the recovery data the aquifer transmissivity is calculated to be 1.8 m²/day. The average transmissivity of the bedrock aquifer in the area of the test well is calculated to be 5.2 m²/day. At the end of pumping, it required 8 minutes for 98 percent recovery of the total drawdown in the static water level created during pumping.

Based on the data obtained during the pumping test, it can be concluded that the well is capable of sustaining a short term yield of at least 65 litres per minute (14 lpm), and that during the course of the six hour pumping period only about 84 percent of the available drawdown in the test well was utilized.

4.3.7 Interference Effects

During the pumping of TW 2, periodic water level measurements were made at TW 1 and TW 3, and during the pumping of TW 4, periodic water level measurements were made at TW 2 and TW 3 in order to assess the potential interference effects between the wells. A maximum drawdown of 0.03 metres and 0.07 metres was measured at TW 1 and TW 3, respectively, during the pumping of TW 2. No drawdown was measured at TW 2 and TW 3 during the pump test at TW 4. TW 2 is some 420 and 730 metres from TW 1 and TW 3, respectively, and TW 4 is some 320 and 370 metres from TW 2 and TW 3, respectively.

In order to estimate the maximum interference between future wells at the site, the maximum drawdown measured at the non pumped wells during the pumping of the test wells was used along with the relationship that the drawdown at a well is directly related to the pumping rate. The average drawdown at the test wells was calculated for a thirty year pumping rate of 1100 litres per day which allows for four persons per household. Calculations of expected 30 year drawdown are provided below.

Test Well	TW1	TW2	TW3	TW4	TW5	TW6
30 Year Drawdown Extrapolation of drawdown curves (metres)	4.9	14.5	0.5	1.0	0.7	20.0
30 Year Drawdown Adjusted to 1100 L/D	0.033	0.135	0.003	0.007	0.005	0.230
Average adjusted 30 year drawdown	0.033	0.135	0.003	0.007	0.005	0.230/6 = 0.07 metres

Conservatively, assuming that each well causes an average 30 year drawdown of 0.07 metres at a centrally located well within the proposed subdivision, the total drawdown at the centrally located well due to the interference from the other 66 wells plus the drawdown at the well itself is (0.07 x 67 wells) or 4.7 metres which is acceptable given the available drawdown at each of the test wells.

4.4 Groundwater Flow Directions

Five monitoring wells were installed at the site as described on the Record of Test Pits, Table I and on the attached Table IV. On December 29, 2004 the water levels were measured at the monitoring wells and at the test wells. The elevation of the ground surface at the monitoring wells and the test wells were supplied to us by the client. It is understood that the topography was developed from on-site topographic control survey data by John Kennedy Surveyors Ltd. (OLS), and stereoscopic elevation model developed by Base Mapping Ltd. using OMNR 1:10,000 scale air photographs, and that the elevations are referenced to Geodetic datum. The results of the groundwater level measurements are shown in the attached Table IV.

Based on the groundwater level measurements and elevation survey described above the groundwater flow direction in the supply aquifer and the receiving aquifer was calculated. The groundwater in the supply aquifer is indicated to flow outward to the north and east from a topographical high area near the centre of the site on the west side as shown on the attached Figure 3. The groundwater flow direction in the receiving aquifer is indicated to be towards the wetland in the south portion of the site as shown on the attached Figure 4, and in general follows the site topography.

4.5 Supply Aquifer Protection

In view of the shallow bedrock conditions encountered at the site a series of extra monitoring wells were installed and the water levels in the monitoring wells measured during pumping of adjacent test wells. This monitoring was carried out to check for any hydraulic connection between the overburden/upper bedrock receiving aquifer and the underlying supply aquifer.

During the pumping of TW 1, TW 2 and TW3 observations of any drawdown in the monitoring wells MW2-1, MW2-2, MW3-1, 3-2 and TP SP6 were made. The observation wells were located within 10 metres of the adjacent test well. About 49,000 to 49,500 litres was pumped from the test wells during the monitoring well observation periods.

The results of the monitoring well observations are provided in the attached Table IV and indicate that no measurable hydraulic connection exists between the receiving aquifer and the supply aquifer.

4.6 Development Impacts and Neighbouring Land Uses

The upper groundwater flow as shown on the attached Figure 4 is indicated to be towards the wetland in the south portion of the site. A buffer zone has been incorporated in the proposed development plans to mitigate any potential impact on the wetland due to the proposed development. Accordingly, no negative impact of the proposed development on neighbouring lands is expected.

The groundwater flow in the supply aquifer is indicated on the attached Figure 3. The groundwater flow is indicated to be from the west and to disperse to the north and east across the site. There is no development of the lands for more than 500 metres to the west of the site. Accordingly, no impact on the supply aquifer is expected from any existing off site sources.

As previously mentioned, a former land fill exists some 400 metres north of the site. The groundwater flow direction in the supply aquifer is toward that landfill and also towards the only development (three dwellings) within 500 metres of the site. Accordingly, no impact on the supply aquifer due to the former landfill or the existing development near the site is expected.

The neighbouring land uses within 500 metres of for the subject site consist of the following:

- North side - former land fill and three single family dwellings, Village of Merrickville further than 500 meters from the site
- East side - undeveloped lands, woodlands
- South side - undeveloped lands, wetlands
- West side - undeveloped lands, woodlands

4.7 Well Construction Methodology

Future wells drilled on the site should be constructed with a minimum 18 metre length of casing through the overburden materials and set at least 1 metre into the sound bedrock. The steel casing placed in the boreholes should be pressure grouted. The material used to seal the annular space could consist of a cement grout which is more resistant to artesian groundwater conditions than commercially available bentonite grout. Cement grout mixtures should be allowed to set for a minimum two day period for normal cement or twelve hours for a high early strength cement prior to advancing the well further into bedrock.

Once the casing has been sealed, the well should be advanced uncased into the bedrock until a water supply of sufficient quantity and quality is encountered. The completed well should then be developed to maximize the yield. The well casings should be completed at least 300 millimetres above finished ground surface and should be fitted with a pitless adapter to facilitate below ground plumbing and electrical connections.

Surface grading should direct surface water away from the well.

4.8 Post Development Monitoring Program

The results of this investigation indicate no existing or expected impact on the groundwater quality at this site due to existing land uses or the proposed development itself. Septic effluent dilution calculations, which by experience are known to be a conservative estimate of actual impact, indicate any septic system impact at the site should be well within Ministry of the Environment requirements. Accordingly, a groundwater monitoring program is not considered necessary for this site.

5.0 SUMMARY AND CONCLUSIONS

Based on the terrain evaluation and groundwater supply investigation at the proposed development and the subsequent analysis of the data collected, the following summary and conclusions are provided:

- 1) Class IV septic sewage disposal systems with partially to fully raised leaching beds will be used at this site depending on the lot specific soil and groundwater conditions. The leaching beds should be constructed to conform to the specifications set out in the Ontario Building Code. It is suggested that imported sand with a percolation rate of between 4 and 8 minutes per centimetre be used to construct the partially to fully raised leaching beds. In situ percolation rate tests and/or gradation analyses should be carried out on any potential sand fill material prior to leaching bed construction in order to verify that the percolation time is acceptable. In shallow bedrock areas, provision of a suitable thickness of silty clay could be required to prevent direct entry of septic effluent into the bedrock. Ontario Building Code approved tertiary treatment systems should be incorporated in the design of the septic systems.

Yours truly,

Morey Houle Chevrier Engineering Ltd.

C. R. Morey
C. R. Morey, P. Eng.

File 041-444



- 2) There is a sufficient groundwater supply in the bedrock aquifer system to satisfy the water requirements of the proposed development. It is indicated that most wells will have to be drilled to depths of about 24 to 37 metres and that individual well yields of about 65 to 114 litres per minute (14 to 25 Imperial gallons per minute) will be typical. However, because it is impossible to predict with certainty the depth at which water-producing fractures will be encountered during drilling, it may be necessary to drill to depths greater than 37 metres on some lots to produce a sufficient water supply.
- 3) The groundwater quality at this site is indicated to be suitable for a potable water supply as it meets all the ODWS concentrations for all health related chemical, physical and bacteriological parameters tested for except iron, hydrogen sulphide, total organic carbon and hardness. Water softeners and manganese green sand filters are indicated to be adequate to lower iron, hydrogen sulphide and hardness to within the ODWS. Sodium levels may be of interest to persons on a sodium restricted diet where ion exchange water softeners are used. In that case a separate unsoftened water supply could be used for drinking and culinary purposes to reduce sodium intake.
- 4) Mutual water level interference effects between neighbouring wells in the proposed subdivision are expected to be minimal.
- 5) Future wells drilled on this property should be constructed with casing through the overburden materials and set a minimum of one metre into the sound bedrock. The annulus of the casing should be grouted using the pressure injection method. Casing and grouting should extend to at least 18 metres below the existing ground surface. Wells should be located at least 15 to 18 metres from septic fields for inground and raised bed, respectively, and upgradient of septic fields.
- 6) Based on the impact assessment, the septic systems at the proposed 80 lots at this site are indicated to result in the impact on the groundwater quality at the site boundaries to be within acceptable limits established by the MOE.
- 7) It is considered that the type of existing surrounding land use adjacent to the subject property should not impact the subject site from a water supply or water quality point of view.
- 8) The results of the investigation indicate that no measurable hydraulic connection exists between the receiving aquifer and the supply aquifer.

TABLE I
 RECORD OF TEST PITS
 PROPOSED MERRICKVILLE ESTATES SUBDIVISION
 SCOTCH LINE ROAD, MERRICKVILLE, ONTARIO

TEST PIT NUMBER	DEPTH (METRES)	DESCRIPTION
TP1	0.00 - 0.18	TOPSOIL
	0.18	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP2	0.00 - 0.20	TOPSOIL
	0.20 - 0.66	Red brown fine to medium SAND
	0.66	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP3	0.00 - 0.15	TOPSOIL
	0.15 - 0.33	Red brown fine to medium SAND, some gravel
	0.33	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004

TABLE I

RECORD OF TEST PITS (CONTINUED)

TEST PIT NUMBER	DEPTH (METRES)	DESCRIPTION
TP4	0.00 - 0.25	TOPSOIL
	0.25	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP5	0.00 - 0.20	TOPSOIL
	0.20 - 0.60	Yellow brown fine to medium SAND, some cobbles, trace silt
	0.60	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP6	0.00 - 0.30	TOPSOIL
	0.30 - 0.60	Red brown SILTY SAND, some gravel and cobbles
	0.60 - 1.20	Grey brown SAND and GRAVEL, some cobbles
	1.20 - 2.26	Grey brown SILTY SAND some gravel and cobbles, trace clay (GLACIAL TILL)
	2.26	End of test pit

Test pit dry upon completion of excavating, November 4, 2004. Installed standpipe to 2.2 metres depth, 50 millimetre diameter PVC slotted in lower 1.5 metres and backfilled with native materials.

TABLE I

RECORD OF TEST PITS (CONTINUED)

TEST PIT NUMBER	DEPTH (METRES)	DESCRIPTION
TP7	0.00 - 0.25	TOPSOIL
	0.25 - 0.43	Grey brown SILTY SAND, some gravel
	0.43	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP8	0.00 - 0.20	TOPSOIL
	0.20	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP9	0.00 - 0.20	TOPSOIL
	0.20 - 0.41	Red brown fine SAND, some silt
	0.41	End of test pit, BEDROCK
Test pit dry upon completion of excavating, November 4, 2004		
TP10	0.00 - 0.30	TOPSOIL
	0.30 - 0.84	Grey brown SILTY SAND, some gravel trace clay (GLACIAL TILL)
	0.84	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004. Installed standpipe to 0.8 metres depth, 50 millimetre diameter PVC slotted full length and backfilled with native materials.

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptville, ON
 K0G 1J0

Report Number: 2500525
 Date: 2005-01-20
 Date Submitted: 2005-01-11

Attention: Mr. Randy Morey

Project:

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID:		UNITS	MDL	GUIDELINE		
	Sample Date:	Sample ID:			TYPE	LIMIT	UNITS
Alkalinity as CaCO3	5	253	mg/L	0.001	258	360	
Chloride	1	12	mg/L	1	14	847	
Colour	2	<2	TCU		<2	<2	
Conductivity	5	534	uS/cm		541	3460	
Dissolved Organic Carbon	0.5	1.6	mg/L		1.4	1/2	
Fluoride	0.10	0.35	mg/L		0.36	0/20	
Hydrogen Sulphide	0.01	0.03	mg/L		<0.01	<0.01	
N-NH3 (Ammonia)	0.02	0.05	mg/L		0.05	<0.02	
N-NO2 (Nitrite)	0.10	<0.10	mg/L		<0.10	<0.10	
N-NO3 (Nitrate)	0.10	<0.10	mg/L		<0.10	0.60	
pH		7.72			7.71	7.45	
Phenols	0.001	<0.001	mg/L		<0.001	<0.001	
Sulphate	1	30	mg/L		26	171	
Tannin & Lignin	0.1	<0.1	mg/L		<0.1	<0.1	
TDS (COND - CALC)	5	347	mg/L		352	2210	
Total Kjeldahl Nitrogen	0.05	0.13	mg/L		0.18	0.24	
Turbidity	0.1	19.5	NTU		7.6	6.2	
Hardness as CaCO3	1	280	mg/L		287	566	
Ion Balance	0.01	0.98			0.99	1.00	
Calcium	1	71	mg/L		72	183	
Magnesium	1	25	mg/L		26	27	
Potassium	1	3	mg/L		3	3	
Sodium	2	5	mg/L		5	532	
Iron	0.01	0.93	mg/L		0.64	0.45	
Manganese	0.01	0.04	mg/L		0.03	0.03	

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL:

Ewan McRobbie
 Ewan McRobbie
 Inorganic Lab Supervisor

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptville, ON
 K0G 1J0

Attention: Mr. Randy Morey

Report Number: 2424857
Date: 2005-01-04
Date Submitted: 2004-12-30

Project: 041-474

P.O. Number:
Matrix: Water

PARAMETER	LAB ID:		MDL	UNITS	TYPE	LIMIT	UNITS
	Sample Date:	Sample ID:					
Total Coliforms	362754	362755	0	cf/100mL	MAC	0	cf/100mL
Escherichia Coli	2004-12-29	2004-12-29	0	cf/100mL	MAC	0	cf/100mL
Heterotrophic Plate Count	-HR3	HR6	0	cf/1mL	MAC	500	cf/1mL
Faecal Coliforms	7W2	7W2	0	cf/100mL	MAC	0	cf/100mL
Faecal Streptococcus			0	cf/100mL	MAC	0	cf/100mL
MCE REG. 170/03							

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL: *Krista Quantrell*
 Krista Quantrell
 Microbiology Analyst

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kempville, ON
 K0G 1J0

Report Number: 2500523
 Date: 2005-01-13
 Date Submitted: 2005-01-11

Attention: Mr. Randy Morey

Project:

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID:		UNITS	MDL	363902		363903		363904		TYPE	LIMIT	UNITS
	Sample Date:	Sample ID:			2005-01-09	041-444 TW1	2005-01-09	041-444 TW1	2005-01-10	031-532 TW1			
Total Coliforms			cf/100mL		0		0		31				
Escherichia Coli			cf/100mL		0		0		0				
Heterotrophic Plate Count			cf/1mL		280		20		40				
Faecal Coliforms			cf/100mL		0		0		0				
Faecal Streptococcus			cf/100mL		0		0		0				

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

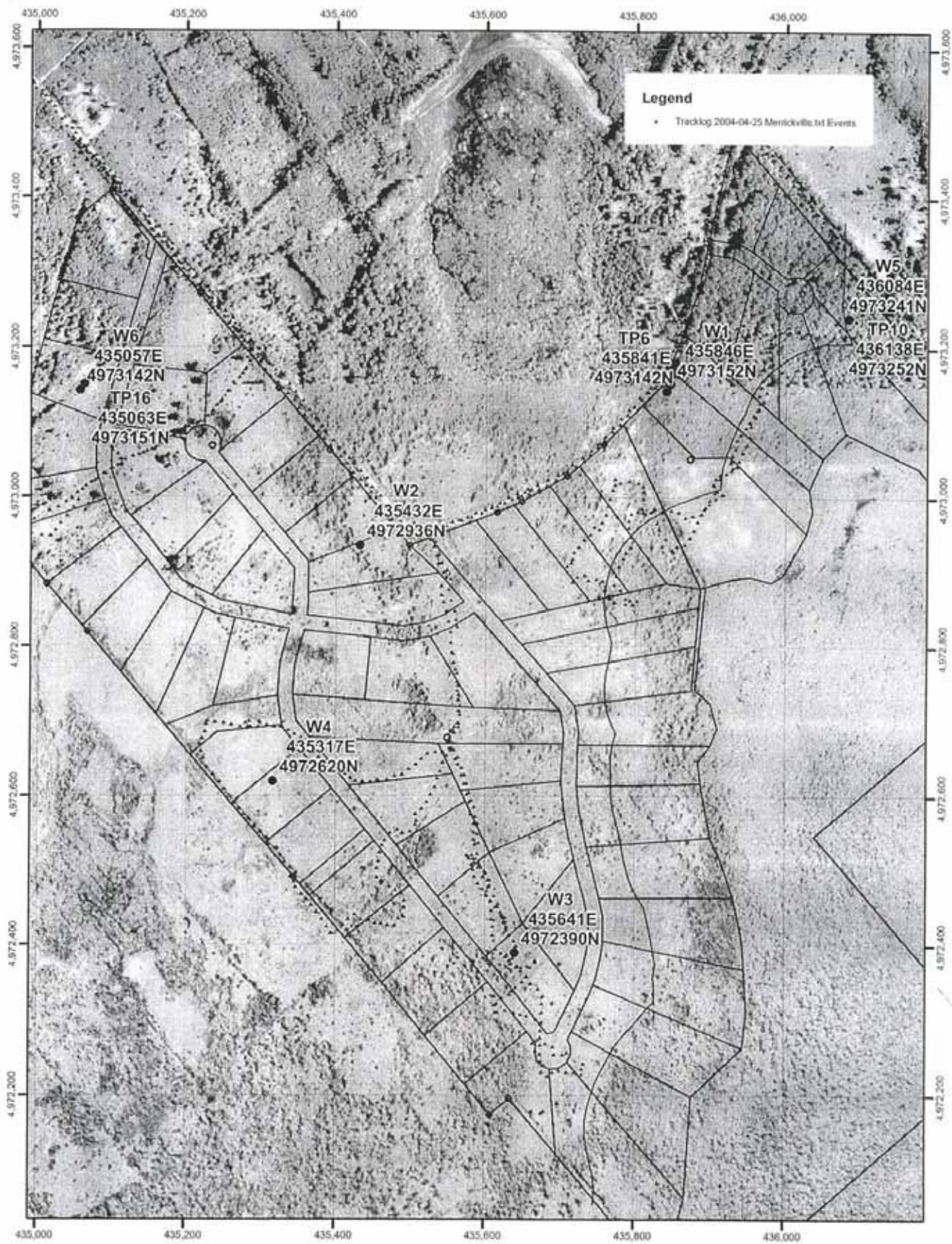
APPROVAL: *Krista Quantrell*
 Krista Quantrell
 Microbiology Analyst

February 2005

041-444

APPENDIX B

RESULTS OF LABORATORY TESTING OF
TEST WELL WATER SAMPLES



1:6,500

Hydro Geology - Planning Wells - Nov 2004

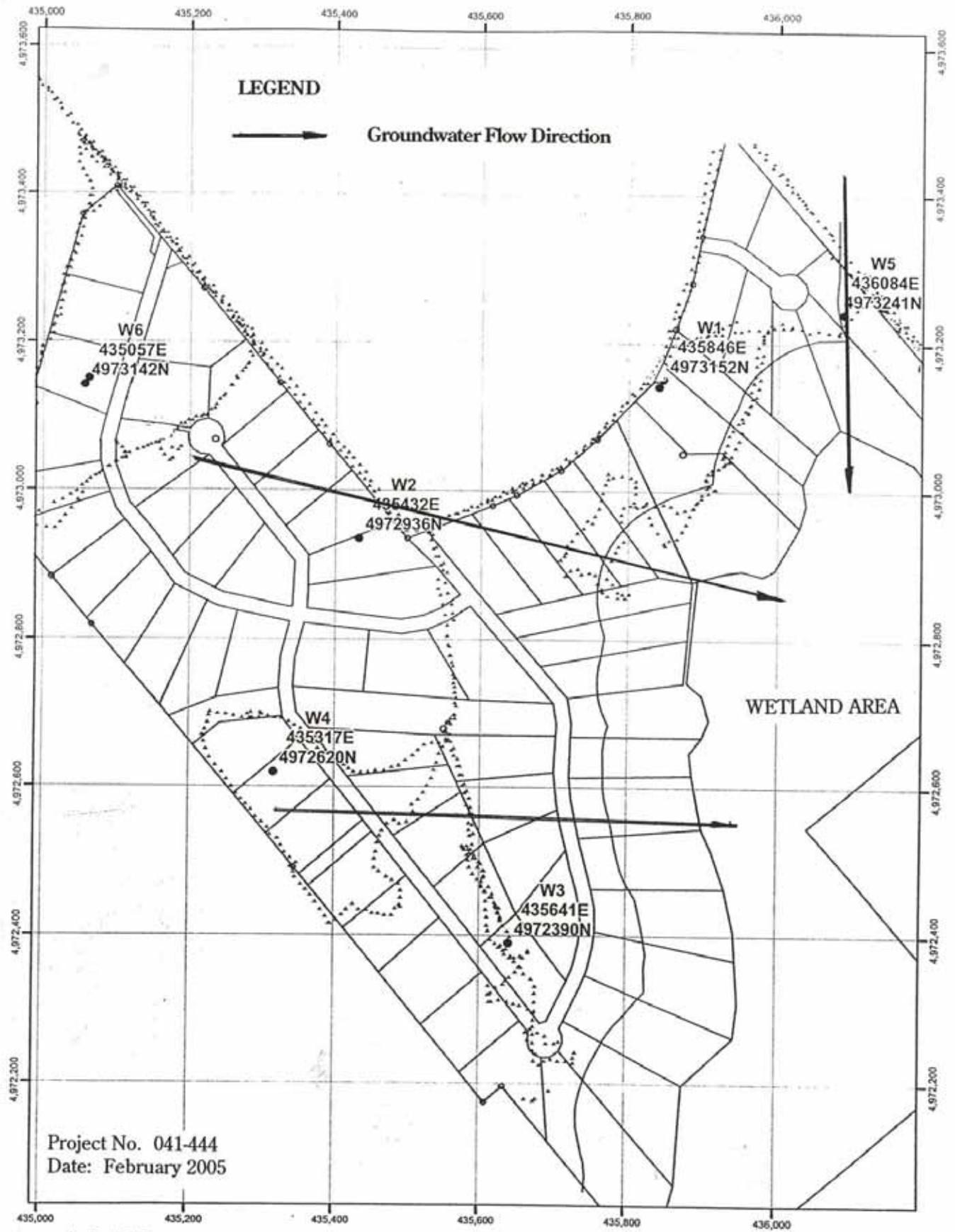
February 2005

041-444

APPENDIX A
TEST WELL LOCATIONS
WITH NORTHINGS AND EASTINGS
PROVIDED BY
MR. C. FOURNIER, P. ENG.

GROUNDWATER FLOW IN RECEIVING AQUIFER

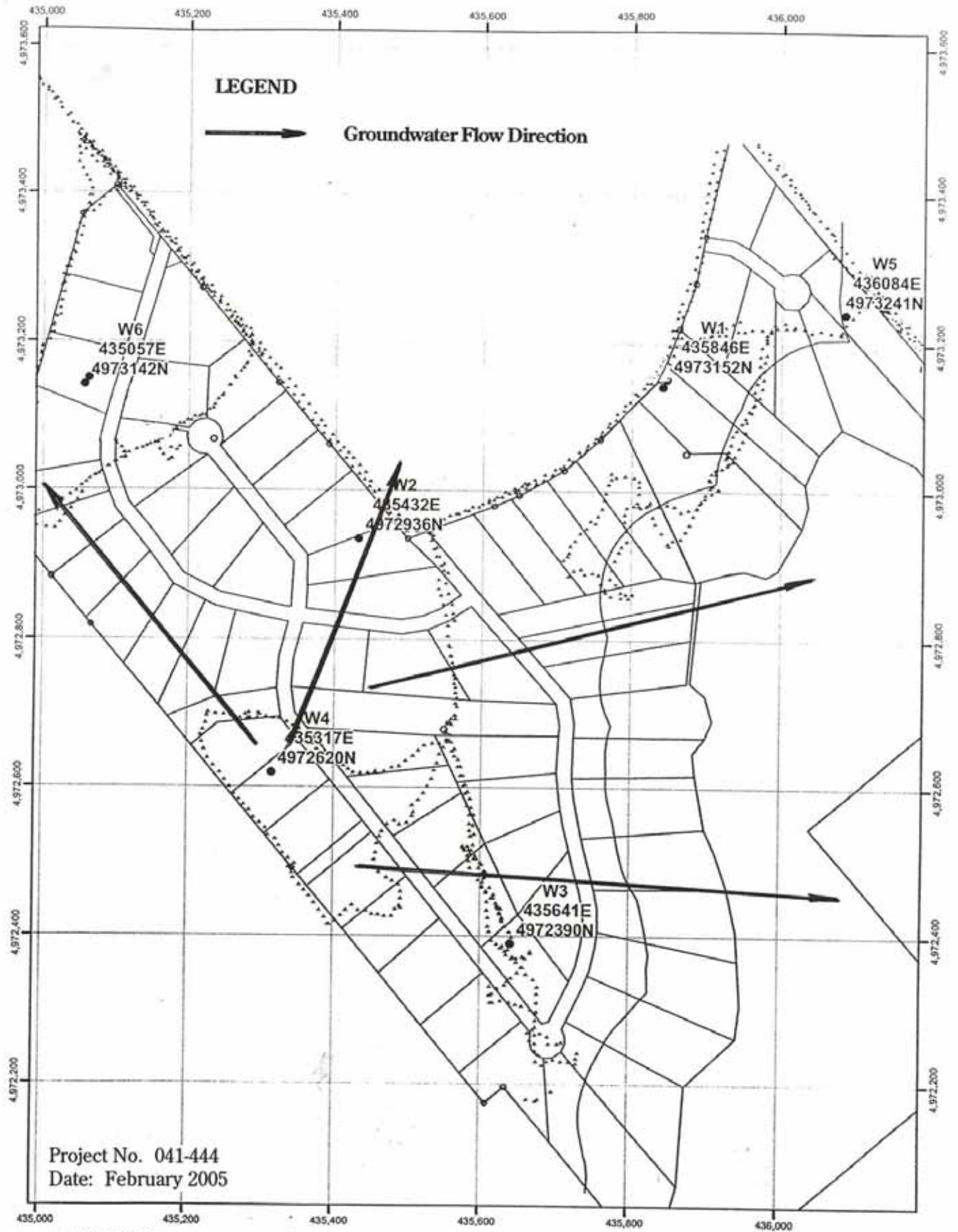
FIGURE 4



1:6,500

GROUNDWATER FLOW IN SUPPLY AQUIFER

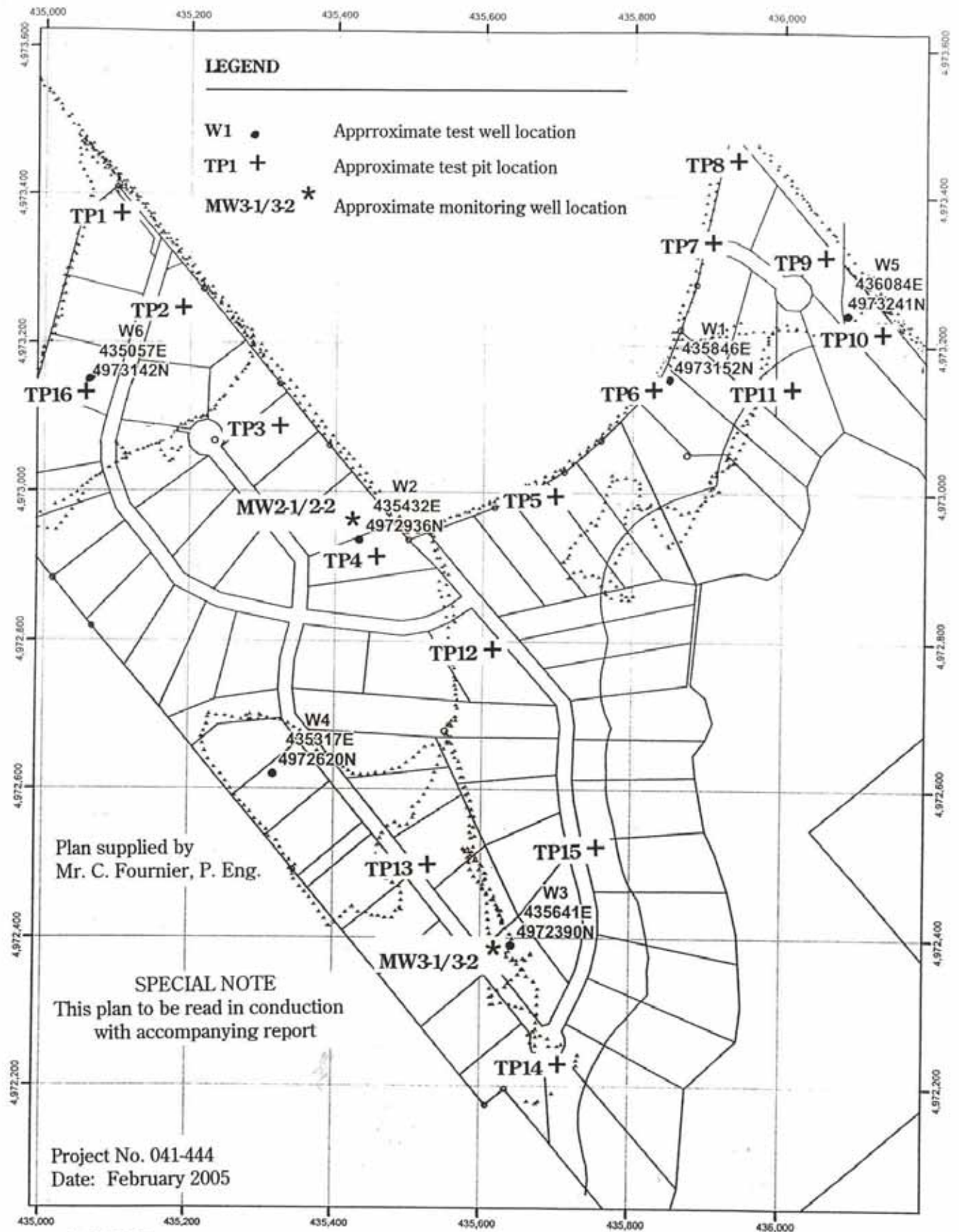
FIGURE 3



Project No. 041-444
Date: February 2005

1:6,500

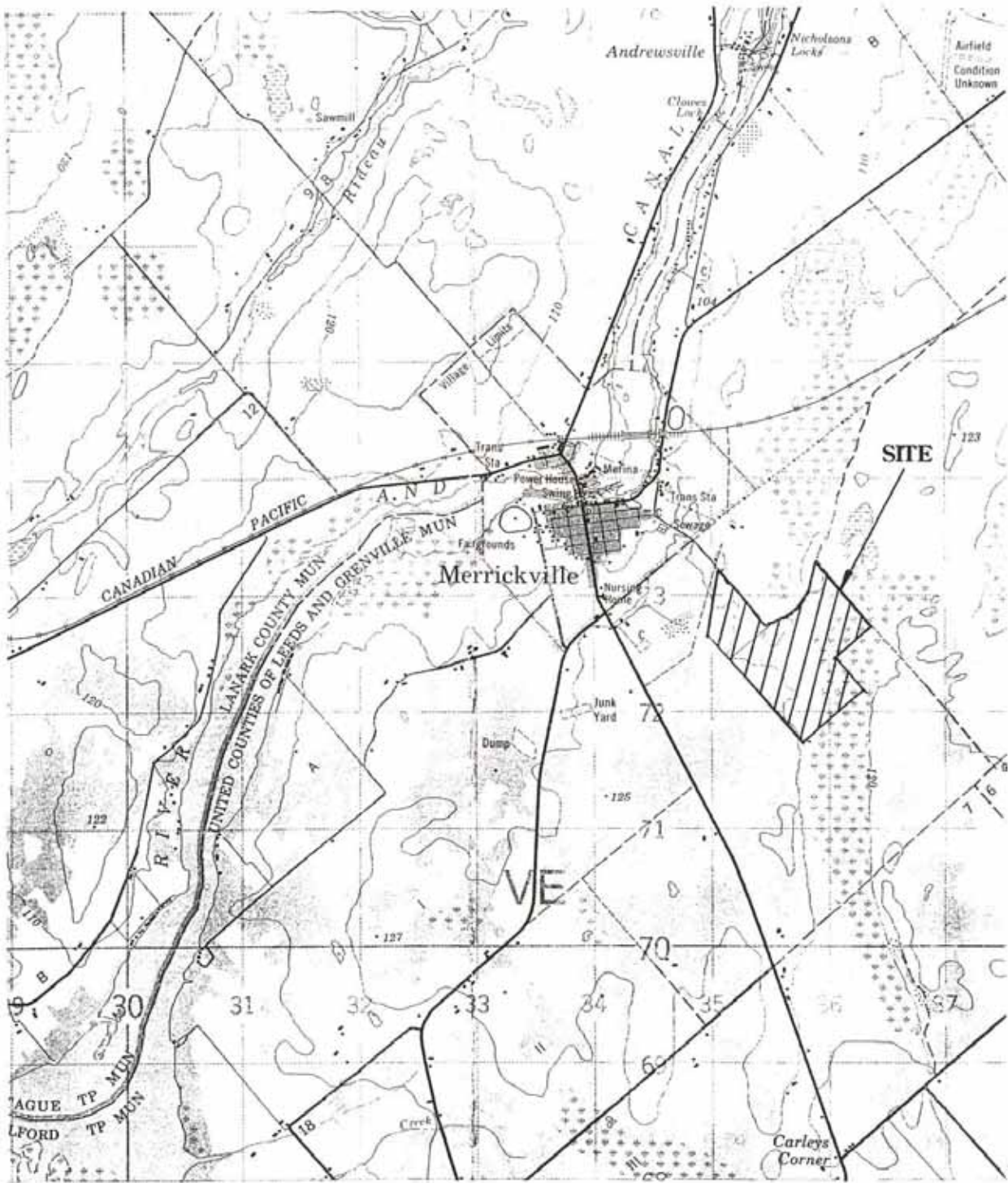
SITE PLAN FIGURE 2



1:6,500

KEY PLAN

FIGURE 1



SCALE: 1:50,000

Project No. 041-444
Date: February 2005

MOREY HOULE CHEVRIER ENGINEERING LTD.

TABLE V
RESULTS OF GROUNDWATER LEVEL MEASUREMENTS
(December 29, 2004)

	Water Level below top of casing (metres)
MW 2-1 (Elev. 118)	frozen
MW 2-2 (Elev. 118)	2.55
MW 3-1 (Elev. 118)	2.70
MW 3-2 (Elev. 118)	2.70
TP 6 - SP (Elev. 116)	1.50
TP 10 -SP (Elev. 116)	0.42
TW1 (Elev. 116)	2.03
TW2 (Elev. 118)	-0.40
TW3 (Elev. 118)	1.95
TW4 (Elev. 124)	4.72
TW5 (Elev. 116)	3.75
TW6 (Elev. 119)	5.46

TABLE IV (CONTINUED)

TIME SINCE START OF PUMPING (MINUTES)	DRAWDOWN (METRES)							
	TW1	TP6-SP	TW2	MW2-1	MW2-2	TW3	MW3-1	MW3-2
20	3.04	0.00						
180	3.17	0.00						
197	3.17		0.00	frozen	0.00			
207	3.17					0.01	0.00	0.00
240	3.18	0.00						
360	3.21	0.00						
373	3.21		0.03	frozen	0.00			
375	3.21					0.02	0.00	0.00
444	3.24	0.00						

ABOUT 49,500 LITRES PUMPED FROM TW 1 DURING OBSERVATION PERIOD

Log of Monitoring Well 2

0.0-9.1 metres grey limestone, two standpipes installed, 50mm PVC pipe with screen 8.2m to 9.1m then solid riser to surface, 50mm PVC pipe installed with screen 5.2 m to 6.1 m then solid riser to surface, backfilled with sand 9.1m to 7.6m, hole plug 7.6m to 6.1m , sand 6.1m to 0.6m, hole plug 0.6m to 0.0m

Log of Monitoring Well 3

0.0-9.1 metres grey limestone, two standpipes installed, 50mm PVC pipe with screen 8.2m to 9.1m then solid riser to surface, 50mm PVC pipe installed with screen 5.2 m to 6.1 m then solid riser to surface, backfilled with sand 9.1m to 7.6m, hole plug 7.6m to 6.1m , sand 6.1m to 0.6m, hole plug 0.6m to 0.0m

TABLE IV
 MONITORING WELL OBSERVATIONS
 MERRICKVILLE ESTATES
 TOWNSHIP OF MERRICKVILLE-WOLFORD, ONTARIO

TIME SINCE START OF PUMPING (MINUTES)	DRAWDOWN (METRES)		
	TW3	MW3-1	MW3-2
4	0.06	0.00	0.00
60	0.14	0.00	0.00
120	0.17	0.00	0.00
300	0.18	0.00	0.00
360	0.18	0.00	0.00
420	0.18	0.00	0.00
480	0.18	0.00	0.00

ABOUT 49,000 LITRES PUMPED FROM TW 3 DURING OBSERVATION PERIOD

TIME SINCE START OF PUMPING (MINUTES)	DRAWDOWN (METRES)							
	TW2	MW2-1	MW2-1	TW3	MW3-1	MW3-1	TW1	TP6-SP
21	11.28	0.00	0.00					
41	11.96	0.00	0.00					
128	12.34	0.00	0.00					
138	12.39			0.01	0.00	0.00		
153	12.43						0.00	0.00
253	12.32	0.00	0.00					
308	12.47						0.00	0.00
318	12.47			0.03	0.00	0.00		
378	12.52	0.00	0.00					
466	12.58						0.02	0.00
478	12.58			0.04	0.00	0.00		
600	12.62						0.03	0.00
613	12.62			0.07	0.00	0.00		
624	12.63	0.00	0.00					

ABOUT 49,000 LITRES PUMPED FROM TW 2 DURING OBSERVATION PERIOD

TABLE II (CONTINUED)

Test Well	Hours Since Pumping Started	Temp. (°C)	Conductivity (uS/cm)	pH (pH units)	Turbidity (NTU)	Free Chlorine	Sulphide
TW 5	1	9.1	165	8.1	0.2	ND	ND
	2	8.1	119	7.8	0.1	ND	ND
	3	-	-	-	-	-	-
	4	7.3	143	7.8	0.2	ND	ND
	5	7.6	130	7.6	0.2	ND	ND
	6	7.0	146	7.0	0.2	ND	ND
TW 6	1	7.9	156	8.0	0.6	ND	ND
	2	-	-	-	-	-	-
	3	10.7	259	8.0	0.2	ND	ND
	4	9.3	250	7.8	0.2	ND	ND
	5	10.8	202	7.8	0.3	ND	ND
	6	7.8	190	7.8	0.2	ND	ND

ND = not detected D = detected

TABLE III

SUMMARY OF PUMPING TEST RESULTS AND WELL PARAMETERS

Well	Tp	Tr	Tav	Q	SC	ho	hf	Td	TD	CS
TW 1	250.1	200.1	225.1	161	50	2.63	5.87	3.24	36.6	0.6
TW 2	43.2	1.8	22.5	114	9	0.20	12.83	12.63	30.5	0.6
TW 3	375.2	150.0	262.3	147	817	2.65	2.83	0.18	30.5	0.7
TW 4	142.9	200.1	171.5	164	309	5.19	5.72	0.53	30.5	0.5
TW 5	500.3	300.2	400.2	164	586	4.45	4.73	0.28	24.4	0.7
TW 6	8.6	1.8	5.2	94	7	5.93	19.46	13.53	24.4	0.5

Note: Tp: Transmissivity as calculated from pumping data (m^2/day)
Tr: Transmissivity as calculated from recovery data (m^2/day)
Tav: Average transmissivity (average of pumping and recovery) (m^2/day)
Q: Test pumping rate (m^3/day)
SC: Specific Capacity ($m^3/day/m$)
ho: Static water level (below top of casing) at beginning of pumping test (metres)
hf: Water level (below top of casing) at end of 6 hour pumping test (metres)
Td: Total drawdown (metres)
TD: Total depth of well (below ground surface) (metres)
CS: Casing stickup above ground surface (metres)

TABLE II
RESULTS OF THE FIELD WATER QUALITY MEASUREMENTS
FOR TEST WELLS

Test Well	Hours Since Pumping Started	Temp. (°C)	Conductivity (uS/cm)	pH (pH units)	Turbidity (NTU)	Free Chlorine	Sulphide
TW 1	1	7.3	79	7.8	0.7	ND	ND
	2	-	-	-	-	-	-
	3	9.5	197	8.0	0.0	ND	ND
	4	8.6	197	7.7	0.5	ND	ND
	5	7.7	195	8.5	0.2	ND	ND
	6	7.7	119	7.7	0.2	ND	ND
TW 2	1	9.0	210	7.9	0.1	ND	ND
	2	10.5	178	8.1	0.5	ND	ND
	3	-	-	-	-	-	-
	4	9.1	45	7.9	0.0	ND	ND
	5	9.7	273	7.8	0.1	ND	ND
	6	7.7	141	7.9	0.1	ND	ND
TW 3	1	7.8	198	7.9	-	ND	ND
	2	7.7	304	7.7	-	ND	ND
	3	8.3	310	8.1	-	ND	ND
	4	-	-	-	-	-	-
	5	7.9	177	8.1	0.0	ND	ND
	6	7.9	291	8.0	0.7	ND	ND
	7	7.4	294	8.0	0.1	ND	ND
TW 4	1	6.5	95	8.0	0.2	ND	D
	2	-	-	-	-	-	-
	3	9.5	273	7.8	0.2	ND	D
	4	9.6	303	7.7	0.3	ND	D
	5	9.7	193	7.8	0.1	ND	D
	6	10.0	328	7.7	0.4	ND	D

TABLE I

RECORD OF TEST PITS (CONTINUED)

TEST PIT NUMBER	DEPTH (METRES)	DESCRIPTION
TP11	0.00 - 0.18	TOPSOIL
	0.18 - 0.81	Red brown to yellow brown fine to medium SAND
	0.81	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004

TP12	0.00 - 0.23	TOPSOIL
	0.23	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004

TP 13	0.00 - 0.15	TOPSOIL
	0.15 - 0.28	Yellow brown SILTY SAND some gravel and cobbles, trace clay (GLACIAL TILL)
	0.28	End of test pit

Test pit dry upon completion of excavating, November 4, 2004

TP14	0.00 - 0.15	TOPSOIL
	0.15	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004

TABLE I

RECORD OF TEST PITS (CONTINUED)

TEST PIT NUMBER	DEPTH (METRES)	DESCRIPTION
TP15	0.00 - 0.15	TOPSOIL
	0.15	End of test pit, BEDROCK

Test pit dry upon completion of excavating, November 4, 2004

TP16	0.00 - 0.48	Topsoil and sand (FILL)
	0.48 - 2.13	Red brown fine to medium SAND
	2.13	End of test pit

Test pit dry upon completion of excavating, November 4, 2004. Installed standpipe to 2.1 metres depth, 50 millimetre diameter PVC slotted in lower 1.5 metres and backfilled with native materials.

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptonville, ON
 K0G 1J0

Report Number: 2424B58
 Date: 2005-01-10
 Date Submitted: 2004-12-30

Attention: Mr. Randy Morey

Project: 041-474

P.O. Number:
 Matrix:

PARAMETER	LAB ID:		MDL	UNITS	362756 2004-12-29 -HR3 TW 2	362757 2004-12-29 -HR6 TW 2	LIMIT	UNITS	GUIDELINE
	Sample Date:	Sample ID:							
Alkalinity as CaCO3	5	266	5	mg/L	267		500	mg/L	MCE REG. 170/03
Chloride	1	17	1	mg/L	17		250	mg/L	
Colour	2	<2	2	TCU	<2		5	TCU	
Conductivity	5	548	5	uS/cm	551			TCU	
Dissolved Organic Carbon	0.5	0.5	0.5	mg/L	<0.5		5	mg/L	
Fluoride	0.10	0.37	0.10	mg/L	0.43		1.5	mg/L	
Hydrogen Sulphide	0.01	<0.01	0.01	mg/L	<0.01		0.05	mg/L	
N-NH3 (Ammonia)	0.02	0.08	0.02	mg/L	0.08			mg/L	
N-NO2 (Nitrite)	0.10	<0.10	0.10	mg/L	<0.10		1.0	mg/L	
N-NO3 (Nitrate)	0.10	<0.10	0.10	mg/L	<0.10		10.0	mg/L	
pH		7.52			7.53		6.5-8.5		
Phenols	0.001	<0.001	0.001	mg/L	<0.001				
Sulphate	1	21	1	mg/L	22		500	mg/L	
Tannin & Lignin	0.1	<0.1	0.1	mg/L	<0.1				
TDS (COND - CALC)	5	356	5	mg/L	358		500	mg/L	
Total Kjeldahl Nitrogen	0.05	0.09	0.05	mg/L	0.10				
Turbidity	0.1	5.5	0.1	NTU	5.6		1.0	NTU	
Hardness as CaCO3	1	281	1	mg/L	281		100	mg/L	
Ion Balance	0.01	0.96	0.01		0.95				
Calcium	1	68	1	mg/L	68				
Magnesium	1	27	1	mg/L	27				
Potassium	1	3	1	mg/L	3				
Sodium	2	7	2	mg/L	7		20	mg/L	
Iron	0.01	0.56	0.01	mg/L	0.57		0.3	mg/L	
Manganese	0.01	0.04	0.01	mg/L	0.04		0.05	mg/L	

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

Comment:

APPROVAL:

Ewan McRobbie
 Inorganic Lab Supervisor

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptonville, ON
 K0G 1J0

Report Number: 2423966
 Date: 2004-12-13
 Date Submitted: 2004-12-11

Attention: Mr. Randy Morey

Project:

P.O. Number:
 Matrix:

Water

PARAMETER	UNITS	MDL	LAB ID:		360700		GUIDELINE	
			Sample Date:	Sample ID:	Sample Date:	Sample ID:	TYPE	LIMIT
Total Coliforms	cf/100mL		2004-12-09	TW3	2004-12-09	TW3		
Escherichia Coli	cf/100mL		Dec 9 HR1		Dec 9 HR 6			
Heterotrophic Plate Count	cf/1mL							
Faecal Coliforms	cf/100mL							
Faecal Streptococcus	cf/100mL							
			0		0			
			0		0			
			3		0			
			0		0			
			0		0			

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

Comment:

APPROVAL:

Peter Haulena

Analytical Services Manager
 Results relate only to the parameters tested on the samples submitted for analysis.

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kempthville, ON
 K0G 1J0

Report Number: 2423967
 Date: 2004-12-17
 Date Submitted: 2004-12-11

Attention: Mr. Randy Morey

Project:

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID:		MDL	UNITS	360701	360702	GUIDELINE
	Sample Date:	Sample ID:					
Alkalinity as CaCO3	5		5	mg/L	272	276	
Chloride	1		1	mg/L	44	43	
Colour	2		2	TCU	<2	<2	
Conductivity	5		5	uS/cm	655	658	
Dissolved Organic Carbon	0.5		0.5	mg/L	1.0	0.7	
Fluoride	0.10		0.10	mg/L	0.19	0.24	
Hydrogen Sulphide	0.01		0.01	mg/L	<0.01	<0.01	
N-NH3 (Ammonia)	0.02		0.02	mg/L	0.04	0.03	
N-NO2 (Nitrite)	0.10		0.10	mg/L	<0.10	<0.10	
N-NO3 (Nitrate)	0.10		0.10	mg/L	<0.10	<0.10	
pH					7.68	7.67	
Phenols	0.001		0.001	mg/L	<0.001	<0.001	
Sulphate	1		1	mg/L	24	24	
Tannin & Lignin	0.1		0.1	mg/L	<0.1	<0.1	
TDS (COND - CALC)	5		5	mg/L	426	428	
Total Kjeldahl Nitrogen	0.05		0.05	mg/L	0.12	0.10	
Turbidity	0.1		0.1	NTU	3.2	1.4	
Hardness as CaCO3	1		1	mg/L	340	347	
Ion Balance	0.01		0.01		1.08	1.08	
Calcium	1		1	mg/L	85	86	
Magnesium	1		1	mg/L	31	32	
Potassium	1		1	mg/L	2	2	
Sodium	2		2	mg/L	21	20	
Iron	0.01		0.01	mg/L	0.20	0.19	
Manganese	0.01		0.01	mg/L	0.03	0.03	

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL:

Ewan McRobble
 Inorganic Lab Supervisor

Client: Morey Houle Chevrler Engineering
 28 Clouhier St. E., Unit B, Box 310
 Kemptonville, ON
 K0G 1J0

Attention: Mr. Randy Morey

Report Number: 2502362
 Date: 2005-02-14
 Date Submitted: 2005-02-12
 Project: 041-444

P.O. Number:
 Matrix:

PARAMETER	LAB ID:		UNITS	MDL	TYPE	LIMIT	UNITS
	Sample Date:	Sample ID:					
Total Coliforms	368443	363444	cf/100mL				
Escherichia Coli	2005-02-11	2005-02-11	cf/100mL				
Heterotrophic Plate Count	TW4 HR3 041-444	TW4 HR6 041-444	cf/1 mL				
Faecal Coliforms			cf/100mL				
Faecal Streptococcus			cf/100mL				

MDL = Method Detection Limit INC = Incomplete AG = Analytical Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration



APPROVAL: Peter Haulova

ACCUTEST LABORATORIES LTD

REPORT OF ANALYSIS

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptville, ON
 K0G 1J0

Report Number: 2502363
 Date: 2005-02-17
 Date Submitted: 2005-02-12

Attention: Mr. Randy Morey

Project: 041-444

P.O. Number:
 Matrix: Water

PARAMETER	UNITS	MDL	LAB ID:		TYPE	LIMIT	UNITS
			Sample Date:	Sample ID:			
Alkalinity as CaCO3	mg/L	5	368445	368446			
Chloride	mg/L	1	2005-02-11	2005-02-11			
Colour	TCU	2	TW4 HR3 041-444	TW4 HR6 041-444			
Conductivity	uS/cm	5					
Disolved Organic Carbon	mg/L	0.5					
Fluoride	mg/L	0.10					
Hydrogen Sulphide	mg/L	0.01					
N-NH3 (Ammonia)	mg/L	0.02					
N-NO2 (Nitrite)	mg/L	0.10					
N-NO3 (Nitrate)	mg/L	0.10					
pH							
Phenols	mg/L	0.001					
Sulphate	mg/L	1					
Tannin & Lignin	mg/L	0.1					
TDS (COND - CALC)	mg/L	5					
Total Kjeldahl Nitrogen	mg/L	0.05					
Turbidity	NTU	0.1					
Hardness as CaCO3	mg/L	1					
Ion Balance		0.01					
Calcium	mg/L	1					
Magnesium	mg/L	1					
Potassium	mg/L	1					
Sodium	mg/L	2					
Iron	mg/L	0.01					
Manganese	mg/L	0.01					

MDL = Method Detection Limit, IMC = Incomplete, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Allowable Concentration, IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL
 Ewan M. Robbins
 Inorganic Lab Supervisor

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptville, ON
 K0G 1J0

Report Number: 2502009
 Date: 2005-02-10
 Date Submitted: 2005-02-08

Attention: Mr. Randy Morey

Project: 041-444

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID:		MDL	UNITS	GUIDELINE	
	Sample Date:	Sample ID:			TYPE	LIMIT
Total Coliforms	367427	367428				
Escherichia Coli	2005-02-07	2005-02-07				
Heterotrophic Plate Count	MHCEL	MHCEL				
Faecal Coliforms	HR3	HR6				
Faecal Streptococcus	TWS	TWS				
	0	1		MAC	0	cf/100mL
	0	0		MAC	0	cf/100mL
	4	50		MAC	500	cf/1mL
	0	0		MAC	0	cf/100mL
	0	0		MAC	0	cf/100mL

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL: *Krista Quantrill*
 Krista Quantrill
 Microbiology Analyst

Client: Morey Houle Chevrier Engineering
 28 Clothier St E., Unit B, Box 910
 Kemptonville, ON
 K0G 1J0

Report Number: 2502011
 Date: 2005-02-15
 Date Submitted: 2005-02-08

Attention: Mr. Randy Morey

Project: 041-444

P.O. Number:
 Matrix: Water

PARAMETER	LAB ID:		MDL	UNITS	367430	367431	GUIDELINE
	Sample Date:	Sample ID:					
Alkalinity as CaCO3	5	2005-02-07	5	mg/L	MHCEL	263	MOE REG. 170/03
Chloride	1	MHCEL	1	mg/L	HR3	4	
Colour	2	HR3	2	TCU	HR6	<2	
Conductivity	5	TVS	5	uS/cm	TVS	508	
Dissolved Organic Carbon	0.5		0.5	mg/L		1.9	
Fluoride	0.10		0.10	mg/L		0.26	
Hydrogen Sulphide	0.01		0.01	mg/L		0.02	
N-NH3 (Ammonia)	0.02		0.02	mg/L		<0.02	
N-NO2 (Nitrite)	0.10		0.10	mg/L		<0.10	
N-NO3 (Nitrate)	0.10		0.10	mg/L		<0.10	
pH						7.75	
Phenols	0.001		0.001	mg/L		<0.001	
Sulphate	1		1	mg/L		16	
Tannin & Lignin	0.1		0.1	mg/L		<0.1	
TDS (COND - CALC)	5		5	mg/L		330	
Total Kjeldahl Nitrogen	0.05		0.05	mg/L		0.05	
Turbidity	0.1		0.1	NTU		1.2	
Hardness as CaCO3	1		1	mg/L		283	
Ion Balance	0.01		0.01			0.99	
Calcium	1		1	mg/L		69	
Magnesium	1		1	mg/L		27	
Potassium	1		1	mg/L		<1	
Sodium	2		2	mg/L		<2	
Iron	0.01		0.01	mg/L		0.43	
Manganese	0.01		0.01	mg/L		<0.01	

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

APPROVAL: 
 Ewan McRobbie
 Inorganic Lab Supervisor

Client: Mory Houle Chevrer Engineering
 28 Clothier St. E., Unit B, Box 910
 Kempville, ON
 K0G 1J0

Report Number: 2502168
 Date: 2005-02-11
 Date Submitted: 2005-02-09

Attention: Mr. Randy Morsy

Project: 041-444

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID:		UNITS	MDL	TYPE	LIMIT	UNITS	GUIDELINE
	Sample Date:	Sample ID:						
Total Coliforms	367/R2	367783	cf/100mL		MAC	0	cf/100mL	MOE REG 170/03
Escherichia Coli	2005-02-09	2005-02-08	cf/100mL		MAC	0	cf/100mL	
Heterotrophic Plate Count	HR3	HR6	cf/1mL		MAC	500	cf/1mL	
Faecal Coliforms	TW6	TW6	cf/100mL		MAC	0	cf/100mL	
Faecal Streptococcus			cf/100mL		MAC	0	cf/100mL	

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

APPROVAL

 Kimia Cuanzill

ACCUTEST LABORATORIES LTD

REPORT OF ANALYSIS

Client: Morey Houle Chevrier Engineering
 26 Clozier St E., Unit B, Box 910
 Kamptville, ON
 K0G 1J0

Report Number: 2502169
 Date: 2005-02-16
 Date Submitted: 2005-02-09

Attention: Mr. Randy Morey

Project: 041-444

P.O. Number:
 Matrix:

Water

PARAMETER	LAB ID		UNITS	MDL	367784		367785		367786		TYPE	LIMIT	UNITS
	Sample Date	Sample ID			2005-02-06	2005-02-08	2005-02-08	2005-02-08	HR3	HR6			
Alkalinity as CaCO3			mg/L	5	260	260							
Chloride			mg/L	1	20	21							
Colour			TCU	2	<2	<2							
Conductivity			uS/cm	5	548	558							
Dissolved Organic Carbon			mg/L	0.5	1.4	1.3							
Fluoride			mg/L	0.10	0.23	0.22							
Hydrogen Sulphide			mg/L	0.01	<0.01	<0.01							
N-NH3 (Ammonia)			mg/L	0.02	0.04	0.04							
N-NO2 (Nitrite)			mg/L	0.10	<0.10	<0.10							
N-NO3 (Nitrate)			mg/L	0.10	<0.10	<0.10							
pH					7.63	7.62							
Phenols			mg/L	0.001	<0.001	<0.001							
Sulphate			mg/L	1	19	19							
Tannin & Lignin			mg/L	0.1	<0.1	<0.1							
TDS (COND - CALC)			mg/L	5	357	363							
Total Kjeldahl Nitrogen			mg/L	0.05	0.11	0.06							
Turbidity			NTU	0.1	3.0	1.8							
Hardness as CaCO3			mg/L	1	277	278							
Ion Balance				0.01	0.93	0.91							
Calcium			mg/L	1	58	67							
Magnesium			mg/L	1	26	25							
Potassium			mg/L	1	2	2							
Sodium			mg/L	2	4	4							
Antimony			mg/L	0.001					4				
Arsenic			mg/L	0.001					<0.001				
Barium			mg/L	0.01					<0.001				
Beryllium			mg/L	0.001					0.21				
Boron			mg/L	0.01					<0.001				
Cadmium			mg/L	0.001					0.04				
Chromium			mg/L	0.001					<0.001				

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Inferior Maximum Allowable Concentration

APPROVAL
 Ewan McRobb
 Investigator/Supervisor

ACCUTEST LABORATORIES LTD

REPORT OF ANALYSIS

Client: **Money Houle Chevrier Engineering**
 28 Clothier St E., Unit B, Box 910
 Kempville, ON
 K0G 1J0

Report Number: **2502169**
 Date: **2005-02-16**
 Date Submitted: **2005-02-09**

Attention: **Mr. Randy Morey**

Project: **G41-444**

P.O. Number:

Matrix: **Water**

PARAMETER	UNITS	MDL	367785				TYPE	LIMIT	UNITS
			367784	2005-02-08	367785	367786			
Cobalt	mg/L	0.0002	HR3	HRG	HRG				
Copper	mg/L	0.001							
Cr(VI)	mg/L	0.05							
Iron	mg/L	0.01	0.20						
Lead	mg/L	0.001		0.21					
Manganese	mg/L	0.01	0.03						
Mercury	mg/L	0.0001							
Molybdenum	mg/L	0.005							
Nickel	mg/L	0.005							
Selenium	mg/L	0.001							
Silver	mg/L	0.0001							
Thallium	mg/L	0.0001							
Vanadium	mg/L	0.001							
Zinc	mg/L	0.01							
			HR3	HRG	HRG	VOC			

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective CG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration
 Comment:

APPROVAL

 Ewan MacDougall
 In-charge Lab. Supervisor

ACCU-EST LABORATORIES LTD

REPORT OF ANALYSIS

Client: **Morey Houle Chevrler Engineering**
 26 Clothier St E, Unit B, Box 910
 Kempville, ON
 K0G 1J0

Report Number: 2502159
 Date: 2005-02-16
 Date Submitted: 2005-02-09

Attention: **Mr. Randy Morey**

Project: 041-444

P.O. Number:
 Matrix:

Water

PARAMETER	UNITS	MDL	VOC	357786 2005-02-08 HR6	TYPE	LIMIT	UNITS	GUIDELINE
								Water
Styrene	ug/L	0.5						
t-1,2-Dichloroethylene	ug/L	0.4						
t-1,3-Dichloropropylene	ug/L	0.2						
Tetrachloroethylene	ug/L	0.3						
Toluene	ug/L	0.5						
Trichloroethylene	ug/L	0.3						
Trichlorofluoromethane	ug/L	0.5						
Vinyl Chloride	ug/L	0.5						
VOC SURROGATES								
1,2-dichloroethane-d4	%			97				
4-bromofluorobenzene	%			83				
Toluene-d8	%			100				

MDL = Method Detection Limit INC = Incomplete AO = Analytic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Interim Maximum Allowable Concentration

APPROVAL: 
 Mina Nasir
 Chemist Lab Supervisor

ACCUTEST LABORATORIES LTD

REPORT OF ANALYSIS

Client: Money Houle Chevrer Engineering
 28 Clothier St E, Unit B, Box 910
 Kempsville, ON
 K0G 1J0

Report Number: 2502169
 Date: 2005-02-16
 Date Submitted: 2005-02-09
 Project: 041-444

Attention: Mr. Randy Morey

P.O. Number:
 Matrix: Water

PARAMETER	LAB ID: 357785		UNITS	MDL	VOC	TYPE	LIMIT	UNITS	GUIDELINE
	Sample Date: 2005-02-06	HFIC							
VOLATILE ORGANIC COMPOUNDS - VOCs									
1,1,1,2-tetrachloroethane	ug/L	0.6	<0.6						
1,1,1-trichloroethane	ug/L	0.4	<0.4						
1,1,2,2-tetrachloroethane	ug/L	0.6	<0.6						
1,1,2-trichloroethane	ug/L	0.4	<0.4						
1,1-dichloroethane	ug/L	0.4	<0.4						
1,1-dichloroethylene	ug/L	0.5	<0.5						
1,2-dibromoethane	ug/L	1.0	<1.0						
1,2-dichloroethane	ug/L	0.4	<0.4						
1,2-dichloropropane	ug/L	0.7	<0.7						
1,3,5-trimethylbenzene	ug/L	0.3	<0.3						
1,3-dichlorobenzene	ug/L	0.4	<0.4						
1,4-dibromobenzene	ug/L	0.4	<0.4						
Benzene	ug/L	0.5	<0.5						
Bromodichloromethane	ug/L	0.3	<0.3						
Bromoform	ug/L	0.4	<0.4						
Bromomethane	ug/L	0.5	<0.5						
o-1,2-Dichloroethylene	ug/L	0.4	<0.4						
c-1,3-Dichloropropylene	ug/L	0.2	<0.2						
Carbon Tetrachloride	ug/L	0.5	<0.5						
Chloroethane	ug/L	1.0	<1.0						
Chloroform	ug/L	0.5	<0.5						
Chloromethane	ug/L	1.0	<1.0						
Dibromochloromethane	ug/L	0.3	<0.3						
Dichloromethane	ug/L	4.0	<4.0						
Ethylbenzene	ug/L	0.5	<0.5						
m/p-xylene	ug/L	1.0	<1.0						
Monochlorobenzene	ug/L	0.7	<0.7						
o-xylene	ug/L	0.5	<0.5						

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IMAC = Inform Maximum Allowable Concentration

APPROVAL

 Miral Nasir
 Organic Lab Supervisor

February 2005

041-444

APPENDIX C

WELL RECORDS PROVIDED BY WELL DRILLER

TW 1 199 0'

Instructions for Completing Form

- For use in the Province of Ontario only. This document is a permanent legal document. Please retain for future reference.
- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-325-6259.
- All metre measurements shall be reported to 1/10th of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

Well Name 1605861	Legal Name ONTARIO LTD	Mailing Address (Street Number/Name, RR, Lot, Concession) 4273 GREEN GABLES LANE
County/District/Municipality LANARK	Township/City/Town/Village LANARK	Province Postal Code Telephone Number (include area code) Ontario K1V 1S4
Address of Well Location (County/District/Municipality) LANARK		Lot Concession 7 1
RR/Street Number/Name		Size/Concession/Block/Tract etc.
IPS Reading 8.3	NAD Zone Easting 118 435846	Northing 4973157
Type of Well 4573157		Mode of Operation Magellan

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth From	Depth To
gray	rocky clay			0	2.13
	limestone		broken	2.13	36.6

Hole Diameter		
Depth From	Metres To	Diameter Centimetres
0	36.6	15.55

Water Record	
Water Type (Metres)	Kind of Water
32.0	Fresh <input checked="" type="checkbox"/> Sulphur <input type="checkbox"/> Salty <input type="checkbox"/> Minerals <input type="checkbox"/>
34.1	Fresh <input checked="" type="checkbox"/> Sulphur <input type="checkbox"/> Salty <input type="checkbox"/> Minerals <input type="checkbox"/>
After test of well yield, water was: <input checked="" type="checkbox"/> Clear and without any odor <input type="checkbox"/> Other (specify)	
Chlorinated <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	

Construction Record					
Inside diam. centimetres	Material	Wall thickness centimetres	Depth From	Depth To	Metres
Casing					
15.88	Steel Fibreglass	4.8	0	18.3	
Screen					
	Steel Fibreglass				
No Casing or Screen					
			17.7	36.6	

Test of Well Yield Record Fee: 25				
Pumping test method	Draw Down Time min	Water Level Metres	Recovery Time min	Water Level Metres
Sub pump				
Pumping rate (litres/min)	24.4	2.63	5.87	
Recovery rate (litres/min)	113	4.60	2.95	
Duration of pumping (hrs & min)	7 hrs & 24 min	3.15	2	
Final water level end of pumping (metres)	5.9	3	3	
Recommended pump type	4	5.47	4	2.87
Recommended pump depth (metres)	33.5	5.54	6	2.84
Recommended pump rate (litres/min)	136	5.63	10	
Recovery rate (litres/min)	20	5.67	15	
Recovery rate (litres/min)	25	5.68	25	2.80
Recovery rate (litres/min)	30	5.69	30	
Recovery rate (litres/min)	40	5.71	40	
Recovery rate (litres/min)	50	5.72	50	
Recovery rate (litres/min)	60	5.73	60	

Plugging and Sealing Record	
Depth set at (Metres)	Material and type (cement, clay, neat cement slurry)
17.7	neat cement slurry

Method of Construction			
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Rotary (air)	<input type="checkbox"/> Diamond	<input type="checkbox"/> Pigging
<input type="checkbox"/> Rotary (conventional)	<input type="checkbox"/> Air percussion	<input type="checkbox"/> Jetting	<input type="checkbox"/> Other
<input type="checkbox"/> Rotary (inverted)	<input type="checkbox"/> Boring	<input type="checkbox"/> Other 2	

Water Use			
<input type="checkbox"/> Domestic	<input type="checkbox"/> Industrial	<input type="checkbox"/> Public Supply	<input type="checkbox"/> Other
<input type="checkbox"/> Stock	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used	
<input type="checkbox"/> Irrigation	<input type="checkbox"/> Municipal	<input type="checkbox"/> Cooling & air conditioning	

Location of Well	
Well No.	Location (show distance of well from road, lot line, and building)
Test Well #1	1.6 km from Collin Rd
2 23194	Date Well Completed 2004 11 21 19

Final Status of Well	
<input type="checkbox"/> Water Supply	<input type="checkbox"/> Recharge well
<input type="checkbox"/> Observation well	<input type="checkbox"/> Abandoned, non-potable supply
<input checked="" type="checkbox"/> Test Hole	<input type="checkbox"/> Abandoned, poor quality

Well Contractor/Technician Information	
Name of Well Contractor A. Rods Drilling Co Ltd	Phone No. (area code & number) 1119
Business Address (street name, number, city etc.) RR #1 Richmond, Ont	
Name of Well Technician (last name, first name) Wesley Dan	Phone No. (area code & number) 172058



Ministry of the Environment

Well Tag Number (Place above and under number below)

Well Record Regulation 903 Ontario Water Resources Act

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Instructions for Completing Form

- For use in the Province of Ontario only. This document is a permanent legal document. Please retain for future reference.
- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-6203.
- All metre measurements shall be reported to 1/10" of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605361, Last Name: ONTARIO LTD, Mapping Address: 4073 GREEN CHARLES LANE, County: GLOUCESTER, Ontario, K1V1S1

Address of Well Location: LANARK, Local Road: MAGELLAN, Lot: 8, Concession: 1

GPS Reading: NAD 83, Zone 18, Easting 485432, Northing 4972936, Magellan

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth From	Depth To
	broken rock			0	0.30
	grey limestone	broken		0.30	30.5

Hole Diameter			Construction Record				Test of Well Yield							
Depth From	Metres To	Diameter Centimetres	Inside diam centimetres	Material	Well thickness centimetres	Depth From	Metres To	Pumping test method	Draw Down	Recovery	Time min	Water Level Metres	Time min	Water Level Metres
0	30.5	15.55	15.88	Concrete	48	0	18.3	Subpump	0.2	12.83	1	9.75	2	7.14
Water Record			Screen				Recovery							
Water Used	Metres	Kind of Water	Outside diam	Material	Well thickness	Depth From	Metres To	Recovery	Time min	Water Level Metres	Time min	Water Level Metres	Time min	Water Level Metres
20	3	Fresh	17.7	Concrete	36	32	32	17.7	30	11.92	30	11.92	40	12.16
After test of well yield, water was			No Casing or Screen				Final Status of Well							
Other and sediment log			Concrete				Unfinished							
Other			17.7				30.5							

Plugging and Sealing Record			Location of Well	
Depth From	Metres To	Material and type	Well ID	Completions
17.7	0	neat cement slurry	23193	2001
Method of Construction			Date Sealed	
Water Use			Date Sealed	
Final Status of Well			Date Sealed	
Well Contractor/Technician Information			Date Sealed	
Name of Well Contractor			Date Sealed	
Business Address			Date Sealed	
Name of Well Technician			Date Sealed	
Signature of Technician			Date Sealed	

Location of Well: Test well #2, 140' depth, 1.2 km N of RR McLean Rd.

Well Tag Number (if applicable, refer to the label)

TW 3

Instructions for Completing Form

- For use in the Province of Ontario only. This document is a permanent legal document. Please retain for future reference.
- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on file. Lack of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-0203.
- All metro measurements shall be reported to 1/10th of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605861 ONTARIO LTD Last Name: ONTARIO LTD Mailing Address (Street Number, Box, PO Box, etc.): 4273 GREEN GABLES LANE

County/District/Municipality: GLoucester Township/City/Town/Village: WOLFORD Province: Ontario Postal Code: K1V 1S4 Telephone Number (include area code): _____

Address of Well Location (County/District/Municipality): LANARK Township: WOLFORD Lot: 8 Concession: _____

RR# Street Number/Name: _____ City/Town/Village: MERRICKVILLE In Compartment/Block/Tract, etc.: _____

GPS Reading: NAD Zone Easting: 18 435993 Northing: 497245 UTM Station Model: magellan Wellhead and Diameter and Capacity: _____

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common mineral	Other Minerals	General Description	Depth (m)	Altitude (m)
	clay			0	0.61
	black grey limestone			0.61	30.5

Hole Diameter

Depth	Metres	Diameter
From	To	Centimetres
0	30.5	155.5

Water Record

Water found at _____ metres Kind of Water: not tested

Gas: not tested Sulphur: _____ Salty: _____ Mineral: _____

Other: _____ Fresh: _____ Sulphur: _____ Early: _____ Mineral: _____

After test of well yield, water was: not tested

Chlorinated: Yes No

Construction Record

Inside diam. Centimetres	Material	Wall thickness Centimetres	Depth From	Metres To
15.88	Steel Fibreglass	4.8	0	18.3
	Concrete			
	Plastic			
	Galvanized			
	Steel Fibreglass			
	Plastic Fibreglass			
	Galvanized			
	Steel Fibreglass			
	Plastic Fibreglass			
	Galvanized			
	Outside diam. Centimetres			
	Steel Fibreglass			
	Plastic Fibreglass			
	Galvanized			
	No Casing or Screen			
			17.7	30.5

Test of Well Yield Rec'd 02/25

Pumping test method	Draw Down	Recovery	
Time min	Water Level Metres	Time min	Water Level Metres
Sub pump			
Pump set at 2.63	Static Level 2.65		2.83
Pumping rate 102	1 2.71	1	2.78
Duration of pumping 8 hrs	2 2.71	2	2.72
Final water level at 10:00 am 8:18 metres	3	3	
Recommenced pump by 4	4 2.71	4	
Performance test with depth 2.7 metres	16 2.72	5	
Stop test pump at 1:36 (10:00 am)	10 2.75	19	
TRF up to 2.71 (10:00 am)	16 2.75	14	2.71
	20 2.75	20	
	25 2.75	25	
If pumping discontinued, state the reason:	30 2.76	30	
	40 2.77	40	
	50 2.78	50	2.65
	60 2.79	60	

Plugging and Sealing Record

Depth: From 17.7 to 0 Metres

Material and type (barrel to slurry, neat cement slurry, etc.): neat cement slurry 4086

Method of Construction

Wash Tool Rotary bits Grouting Drilling

Rotary (conventional) Air percussion Jetting Air

Rotary (reversing) Boring Driving

Water Use

Domestic Industrial Public Supply Irrigation

Stock Commercial Fish raised Other

Irrigation Municipal Cooling & air conditioning

Final Status of Well

Water Supply Recharge well Unfinished Abandoned (Other)

Observation well Abandoned, insufficient supply Dewatering

Test Well Abandoned, poor quality Recharge well



Wall Contractor/Technician Information

Name of Well Contractor: Ac Rock Drilling Ltd License No.: 1119

Business Address (street name, number, city) etc.: 1611 Richmond, Ont

Name of Well Technician (last name, first name): Hogan Dan License No.: T3058

Ministry Use Only

Date Received: _____ Date of Inspection: _____

Inspector: _____

Well Tag Number (Place sticker at end of well casing only)

TVV 4 Page 1 of 1

Instructions for Completing Form

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- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-5203.
- All metre measurements shall be reported to 1/10th of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605861 Last Name: ONTARIO LTD Property Address (Street Number/Name): 4273 GREEN CABLES LANE
 County/District/Municipality: GLoucester Township: WOLFORD City/Village: MERRICKVILLE Province: Ontario Postal Code: K1V 1S4
 Address of Well Location (County/District/Municipality): LANARK Township: WOLFORD City/Village: MERRICKVILLE Lot: 8 Concession: 1
 RR#1/Street Number/Name: LANARK RR#2/Street Number/Name: LANARK Site/Compartment/Block/Tract/etc: LANARK
 GPS Reading: NAD: 1813 Zone: 18 Easting: 435317 Northing: 4972420 Magellan: Magellan

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth (Metres) From	Depth (Metres) To
grey	rocky earth limestone		broken	0	0.30
				0.30	30.5

Hole Diameter				Construction Record				Test of Well Yield					
Depth (Metres) From	Metres To	Diameter (Centimetres)		Inside diam (metres)	Material	Wall thickness (metres)	Depth (Metres) From	Metres To	Pumping test method	Time (min)	Water Level (Metres)	Recovery Time (min)	Water Level (Metres)
0	30.5	15.24		15.88	Concrete	.48	0	18.3	Sub pump	21.3	5.19	5.72	
					Galvanized				Pumping rate (litres/min)	114	5.41	5.34	
					Steel				Duration of pumping (min)	6	5.42	5.34	
					Steel				Time to end of pumping (min)	3			
					Galvanized				Recovery time (min)	4	5.43		
					Concrete				Recovery time (min)	5			
					Concrete				Recovery time (min)	6	5.49		
					Concrete				Recovery time (min)	10	5.64		
					Concrete				Recovery time (min)	18	5.65		
					Concrete				Recovery time (min)	20	5.66		5.25
					Concrete				Recovery time (min)	25	5.67		
					Concrete				Recovery time (min)	30	5.67		5.25
					Concrete				Recovery time (min)	40	5.68		
					Concrete				Recovery time (min)	50	5.69		
					Concrete				Recovery time (min)	60	5.69		

Plugging and Sealing Record

Depth (Metres) From: 17.7 To: 0 Material and type (benzoin slurry, neat cement slurry, etc.): neat cement slurry Annular space: 2724

Method of Construction

Rotary (conventional) Air percussion Drilling Other

Water Use

Domestic Industrial Public Supply Other

Final Status of Well

Unfinished Abandoned (Other) Discontinuing Replacement well



Well Contractor/Technician Information

Name of Well Contractor: Arch Rock Drilling Co Ltd Well Number (on 2 23196): 1119
 Address: 4545 maine, richmond ont
 Name of Well Technician (last name, first name): Hogan Dan Well Tag Number (on 2 23196): T 3058

Ministry Use Only

Date Received: 2005 01 31 Date of Inspection: 2005 01 31
 Remarks: Well Record Number: 1119

Well Tag Number (if pre-1987 and post-1987 - 1988)

Instructions for Completing Form

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- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-6200.
- All metre measurements shall be reported to 1/10th of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605861 Last Name: ONTARIO LTD Mailing Address (Street 13, 14 or part name): 427 GREEN SABLES LANE
 County/District/Municipality: GLUCESTER Township: WOLFORD City/Town/Village: MERICKVILLE Province: Ontario Postal Code: K1V1S4
 Address of Well Location (County District/Municipality): LANARK Township: WOLFORD City/Town/Village: MERICKVILLE Lot: 7 Concession: 1
 RRR/Street Number/Name: GPS Reading: NAD 83 Zone: 18 Easting: 436084 Northing: 493341 Unit: Metres/Feet Mode of Operation: Undersaturated Saturated Differentiated specific

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth From To	DEPTH To
	rocky clay			0	0.91
	grey limestone		Broken	0.91	24.4

Hole Diameter			Construction Record				Test of Well Yield				
Depth From	Metres To	Diameter Centimetres	Inside diam Centimetres	Material	Wall thickness centimetres	Depth From To	Punching test method	Draw Down From	Time min	Recovery Water Level Metres	Water Level Metres
0	24.4	15.23	15.88	1/2" Steel	0.48	0	Subpump	4.45	1	4.7	
Water Record			Screen				Recovery				
Water found at	Kind of Water		Outside diam	Material	Slit size		Final water level end of pumping				
20.7	Not tested						4.7				
21.9	Not tested						4.62				
22.8	Not tested						4.62				
After limit of well yield, water was clear and sediment free. Other specify: Not tested			No casing or screen				Recommended pump rate (litres/min)				
Chlorinated	Yes <input checked="" type="checkbox"/>	No <input type="checkbox"/>	Open hole				17.7 - 24.4				

Plugging and Sealing Record

Depth From To: 17.7 - 0 Material and type (bentonite slurry, seal cement slurry, etc.): neat cement slurry .3178

Method of Construction

Rotary (conventional) Rotary (reversing) Rotary (air) Rotary (percussion) Rotary (other) Drilling Other

Water Use

Domestic Stock Irrigation Industrial Commercial Municipal Public supply Private well Cooling & air conditioning Other

Final Status of Well

Abandoned Sealed Plugged Other Unfinished Abandoned (other) Closed Replaced

Location of Well

In diagram below show location of well from road, lot line, and building. Indicate north by arrow.

Test well # 5. N

Ministry Use Only

Audit No: 2 23195 Date Well Completed: 2005 01 31

Well Contractor/Technician Information

Name of Contractor: A. Kuhn Drilling Co Ltd Well Contractor License No: 1119
 Business Address (Street name, number, city, etc.): 241 Richmond St
 Name of Well Technician (last name, first name): Logan Dan Well Technician's License No: 13058

Ministry Use Only

Date Received: _____ Date of Inspection: _____
 Name: _____



Ministry of the Environment

Well Tag Number (Face sticker and post ready to go)

Well Record

Regulation 903 Ontario Water Resources Act

TW 6 page 1 of 1

Instructions for Completing Form

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- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-6203.
- All metro measurements shall be reported to 1/10" of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605861 Last Name: ONTARIO LTD
 County/District/Municipality: BRUCESTER Township/City/Town/Village: BRUCESTER Province: Ontario Postal Code: K1V1S4
 Mailing Address (Street Number, Name, Box, Lot, Concession): 4373 GREEN GABLES LANE
 Address of Well Location (County/District/Municipality): LANARK Township: WOLFERT City/Town/Village: MERICKVILLE Lot: 8 Concession: 1
 RRA/Street Number/Name: _____
 GPS Position: NAD 83 Zone: 18 Easting: 435057 Northing: 773412 UTM Maker/Model: Magellan

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth From (Metres)	To (Metres)
grey	rocky clay limestone		broken	0	1.22
				1.22	24.4

Hole Diameter		Construction Record				Test of Well Yield					
Depth From (Metres)	Diameter To (Centimetres)	Inside diam (centimetres)	Material	Wall thickness (centimetres)	Depth From (Metres)	To (Metres)	Pumping test method	Draw Down Time (min)	Water Level (Metres)	Recovery Time (min)	Water Level (Metres)
0	21.4	15.23	Concrete	48	0	18.3	Sulphump				
Water Record		Casing		Screen		Pumping test method		Draw Down		Recovery	
Water found at (Metres)	Kind of Water	Material	Thickness (centimetres)	Depth From (Metres)	To (Metres)	Time (min)	Water Level (Metres)	Time (min)	Water Level (Metres)		
18.4	Fresh	Concrete	48	0	18.3	1	5.93	1	19.46		
21.4	Other: salt	Concrete	48	0	18.3	2	7.72	2	15.27		
	Other: sulphur	Concrete	48	0	18.3	3	9.72	3	13.06		
	Other: minerals	Concrete	48	0	18.3	4	13.15	4	9.77		
	Other: other	Concrete	48	0	18.3	5	15.41	5	7.55		
	Other: other	Concrete	48	0	18.3	6	15.41	6	6.17		
	Other: other	Concrete	48	0	18.3	10	16.21	10			
	Other: other	Concrete	48	0	18.3	16	16.41	16			
	Other: other	Concrete	48	0	18.3	20	16.84	20			
	Other: other	Concrete	48	0	18.3	25	17.35	25			
	Other: other	Concrete	48	0	18.3	30	17.62	30			
	Other: other	Concrete	48	0	18.3	40	18.06	40			
	Other: other	Concrete	48	0	18.3	50	17.65	50			
	Other: other	Concrete	48	0	18.3	60	17.65	60			

Plugging and Sealing Record

Depth sealed (Metres): From 12.7 To 0
 Material and type (bentonite slurry, cast cement slurry, etc.): neat cement slurry: 2724
 Method of Construction: Rotary (percussion)
 Water Use: Domestic
 Final Status of Well: Test Hole

Location of Well

In diagram below show the location of well from road, lot line, and building. Indicate in which corner.

Test well #6

46 metres
 4 km
 4 km

Scale: 2 23197
 Date of Well Completed: 2005
 Date of Report: 10/13/05

Well Contractor/Technician Information

Name of Well Contractor: A. Roch, D. W. Gluts
 Address: RR#1 Richmond, Ont
 Name of Well Technician (last name, first name): Maan Dan
 Well Contractor's License No: 1119
 Well Technician's License No: 12058

MW2

Instructions for Completing Form

- For use in the Province of Ontario only. This document is a permanent legal document. Please retain for future reference.
- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-6213.
- All metre measurements shall be reported to 1/10th of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information		MIN		CON		LOT	
First Name 1605861 Ontario Ltd	Last Name	Mailing address (Street Number/Name, RR, E.C. Concession)					
County/District/Municipality Gloucester	Township/City/Town/Village	Province Ontario		Part of Concession K1V 1S4		Telephone Number (include area code)	
Address of Well Location (County, District/Municipality) Lanark		Township Wolford		Lot 8		Concession 1	
R.P.# Street Number/Name		L.R.# Tract/Village Merricks, IL		E.C. Concession/Block/Tract/Unit			
GPS Reading	NAD	Zone	Easting	Northing	Well Make/Model Magellan	Mode of Operation <input checked="" type="checkbox"/> Unattended <input type="checkbox"/> Averaged	Differentiated quality <input type="checkbox"/>

Log of Overburden and Bedrock Materials (see instructions)

General Class	Most common material	Other Material	General Description	Depth from	Depth to
	grey limestone		broken	0	9.1

Hole Diameter		Construction Record				Test of Well Yield			
Depth	Metres	Inside diam	Material	Well Diameter	Depth	Pumping test method	Draw Down	Flow rate	Flow rate
From	To	(centimetres)		(centimetres)	From		min	Metres	min
0	9.1	15.24							
Water Record		Casing				Test of Well Yield			
Water Kind	Kind of Water	2"	Concrete	2-1	0.9	5.2			
Gas	Fresh	2"	Concrete	2-2	0.9	8.2			
Other	Salty								
	Fresh								
	Salty								
	Other								
	Fresh								
	Salty								
	Other								
	Fresh								
	Salty								
	Other								
After test of well yield, water was		Screen				Test of Well Yield			
Clear and free from		Outside diam	Material	2-1	5.2	6.1			
Oil, grease		2"	Concrete	2-2	8.2	9.1			
Other, specify		No Casing or Screen							
<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		<input type="checkbox"/> Open hole							

Plugging and Sealing Record			<input checked="" type="checkbox"/> Annular space	<input type="checkbox"/> Abandonment
Depth of	Interval and type	Material and type	General summary, etc.	
From	To	(sand, clay, rock, cement slurry, etc.)	(cubic metres)	
9.1	7.6	sand		
7.6	6.1	holeplug		
6.1	0.0	sand		
0.0	0.0	holeplug		
Method of Construction				
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Rotary (air)	<input type="checkbox"/> Drilling	<input type="checkbox"/> Digging	
<input type="checkbox"/> Rotary (compressed air)	<input checked="" type="checkbox"/> Air percussion	<input type="checkbox"/> Tapping	<input type="checkbox"/> Other	
<input type="checkbox"/> Rotary (hydraulic)	<input type="checkbox"/> Mining	<input type="checkbox"/> Shoveling		
Water Use				
<input type="checkbox"/> Domestic	<input type="checkbox"/> Industrial	<input type="checkbox"/> Public Supply	<input type="checkbox"/> Other	
<input type="checkbox"/> Stock	<input type="checkbox"/> Commercial	<input type="checkbox"/> Irrigation		
<input type="checkbox"/> Irrigation	<input type="checkbox"/> Municipal	<input type="checkbox"/> Cooling & air conditioning		
Final Status of Well				
<input type="checkbox"/> Water Supply	<input type="checkbox"/> Recharge well	<input type="checkbox"/> Unfinished	<input type="checkbox"/> Abandoned (Other)	
<input checked="" type="checkbox"/> Open, clean well	<input type="checkbox"/> Abandoned - official supply	<input type="checkbox"/> Encroaching		
<input type="checkbox"/> Test Hole	<input type="checkbox"/> Abandoned - other purpose	<input type="checkbox"/> Banked / covered well		



Well Contractor/Technician Information		Ministry Use Only	
Name of Well Contractor Arched Drilling Co Ltd 1119	Well Contractor's Licence No.	Date of Installation	Contractor
Business address (street number, city etc) R.R.#1 Richmond, Ont		2004	112-114
Name of Well Technician (last name, first name) Morgan Dan	Well Contractor's Licence No. 13058	Date Delivered	Year

Well Tag Number (Place sticker and post marker below)

MW3 page 1 of 1

Instructions for Completing Form

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- All Sections must be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-5203.
- All metre measurements shall be reported to 1/10" of a metre.
- Please print clearly in blue or black ink only.

Well Owner's Information and Location of Well Information

First Name: 1605861 Ontario Ltd
Last Name: Green
Address: 1873 Green Sables Lane
City/Town/Village: Gloucester
Province: Ontario
Postal Code: K1V 1S4
Telephone Number: (include area code)
Address of Well Location: Lanark
RR# / Street Number/Name: Walford
Lot: 8
Concession: 1
GPS Reading: NAD 83, Zone 18, Easting 439641, Northing 4572310
Location: Merrickville, Magellan

Log of Overburden and Bedrock Materials (see instructions)

General Colour	Most common material	Other Materials	General Description	Depth From	Depth To
	grey limestone		broken	0	9.1

Hole Diameter	
Depth	Diameter
From	To
0	9.1
	15.24

Water Record	
Water found	Kind of Water
Metres	
0	Fresh
	Salty
	Minerals
	Sulphur
	Other

Construction Record			
Inside diam	Material	Well thickness	Depth
Centimetres		Centimetres	From To
Casing			
2"	Galvanized		(3-1) +0.9 5.2
2"	Galvanized		(3-2) +0.9 8.2
Screen			
			(3-1) 5.2 6.1
2"	Galvanized		(3-2) 8.2 9.1
No Casing or Screen			

Test of Well Yield			
Pumping test method	Draw Down		Recovery
	Time min	Water Level Metres	
Pump make set at (metres)	Start level		
Pump to rate (litres/min)	1		
Depth of pumping (metres)	2		
Final water level end of pumping (metres)	3		
Recommended pump type	4		
Recommended pump depth (metres)	5		
Recommended pump rate (litres/min)	10		
Recommended pump rate (litres/min)	15		
Recommended pump rate (litres/min)	20		
Recommended pump rate (litres/min)	25		
Recommended pump rate (litres/min)	30		
Recommended pump rate (litres/min)	40		
Recommended pump rate (litres/min)	50		
Recommended pump rate (litres/min)	60		

Plugging and Sealing Record			
Depth at	Metres	Material and type	Notes
From	To	(benzotoluene styrene cement slurry) etc.	(if fixed could not see)
9.1	7.6	sand	
7.6	6.1	holeplug	
6.1	0.6	sand	
0.6	0	holeplug	

Location of Well

In diagram below show location of well from road, building and indicate north to arrow.

Monitoring well #3

Method of Construction

Cable Tool
 Rotary (air)
 Rotary (conventional)
 Air percussion
 Rotary (reverse)
 Boring
 Drilling
 Other

Water Use

Domestic
 Stock
 Irrigation
 Industrial
 Commercial
 Municipal
 Public Supply
 Not used
 Cooling & air conditioning

Final Status of Well

Under development
 Downgrading
 Abandoned, poor quality
 Repaired/renovated well
 Plugged
 Other

Well Contractor/Technician Information

Name of Well Contractor: Archibald, W. & Co. Ltd
Address & Phone (street name, number, city etc): Rte 1, Richmond, Ont
Name of Well Technician (full name, first name): Logan, Dan
Signature of Well Contractor: [Signature]
Well Contractor License No.: 1119
Well Technician License No.: 13058

Ministry Use Only

Date Issued: _____
Date Received: _____
Inspector: _____
Inspector License No.: _____

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APPENDIX D
PUMPING TEST DATA
TEST WELL 1

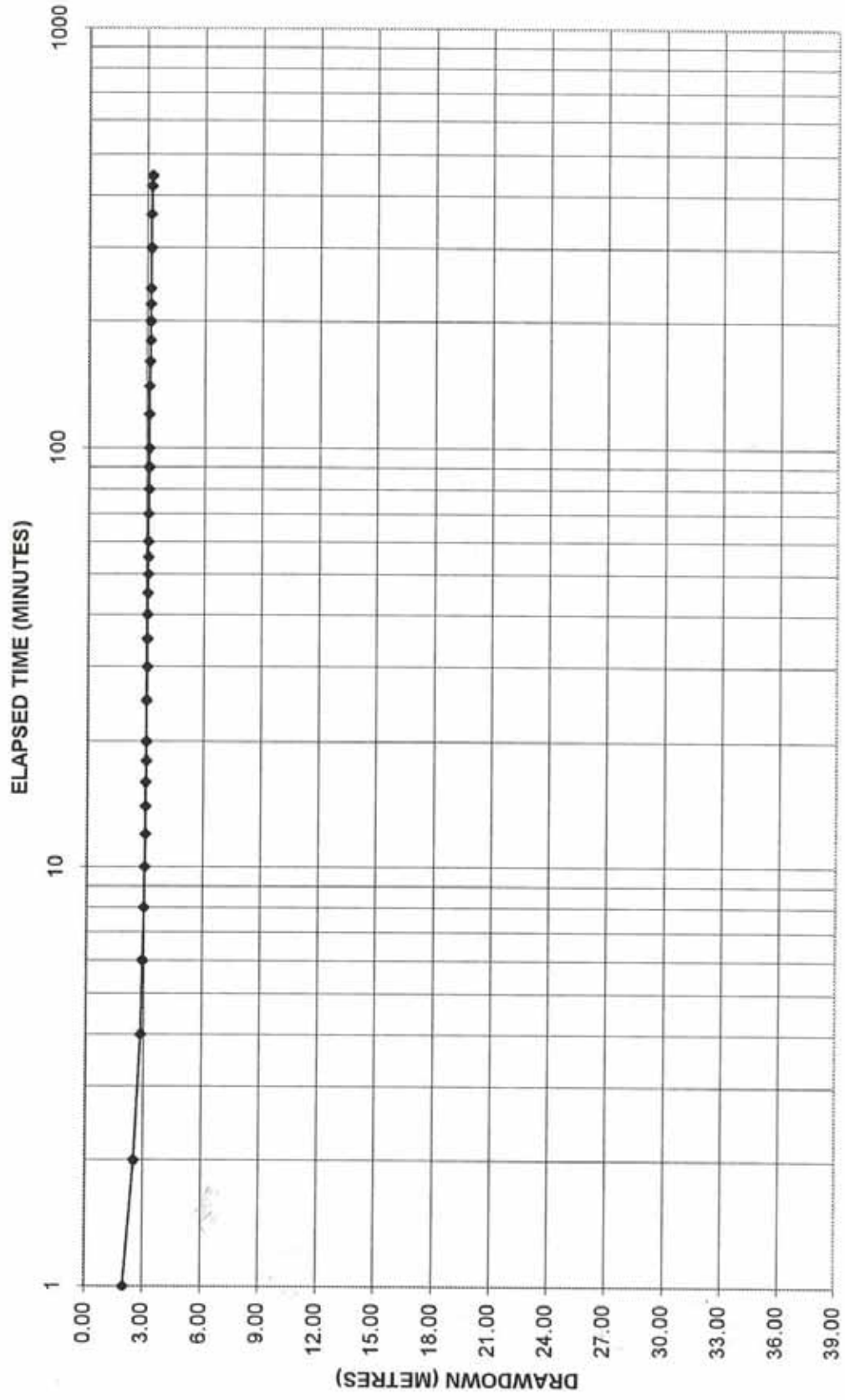
DRAWDOWN DATA
TW1
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of	
			Casing (metres)	Drawdown (metres)
10:47:00	0:00:00	0	2.63	0.00
10:48:00	0:01:00	1	4.60	1.97
10:49:00	0:02:00	2	5.15	2.52
10:51:00	0:04:00	4	5.47	2.84
10:53:00	0:06:00	6	5.54	2.91
10:55:00	0:08:00	8	5.60	2.97
10:57:00	0:10:00	10	5.63	3.00
10:59:00	0:12:00	12	5.64	3.01
11:01:00	0:14:00	14	5.64	3.01
11:03:00	0:16:00	16	5.65	3.02
11:05:00	0:18:00	18	5.66	3.03
11:07:00	0:20:00	20	5.67	3.04
11:12:00	0:25:00	25	5.68	3.05
11:17:00	0:30:00	30	5.69	3.06
11:22:00	0:35:00	35	5.70	3.07
11:27:00	0:40:00	40	5.71	3.08
11:32:00	0:45:00	45	5.71	3.08
11:37:00	0:50:00	50	5.72	3.09
11:42:00	0:55:00	55	5.72	3.09
11:47:00	1:00:00	60	5.73	3.10
11:57:00	1:10:00	70	5.73	3.10
12:07:00	1:20:00	80	5.74	3.11
12:17:00	1:30:00	90	5.74	3.11
12:27:00	1:40:00	100	5.75	3.12
12:47:00	2:00:00	120	5.75	3.12
13:07:00	2:20:00	140	5.76	3.13
13:27:00	2:40:00	160	5.77	3.14
13:47:00	3:00:00	180	5.80	3.17
14:07:00	3:20:00	200	5.80	3.17
14:27:00	3:40:00	220	5.80	3.17
14:47:00	4:00:00	240	5.81	3.18
15:47:00	5:00:00	300	5.82	3.19
16:47:00	6:00:00	360	5.84	3.21
17:47:00	7:00:00	420	5.86	3.23
18:11:00	7:24:00	444	5.87	3.24

Proposed Residential Subdivision

TW1

DRAWDOWN VERSUS LOGTIME



RECOVERY DATA
TW1
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
18:11:00	0:00:00	0	360	0.00	5.87	3.24
18:12:00	0:01:00	1	361	361.00	2.95	0.32
18:15:00	0:04:00	4	364	91.00	2.87	0.24
18:17:00	0:06:00	6	366	61.00	2.84	0.21
18:36:00	0:25:00	25	385	15.40	2.80	0.17

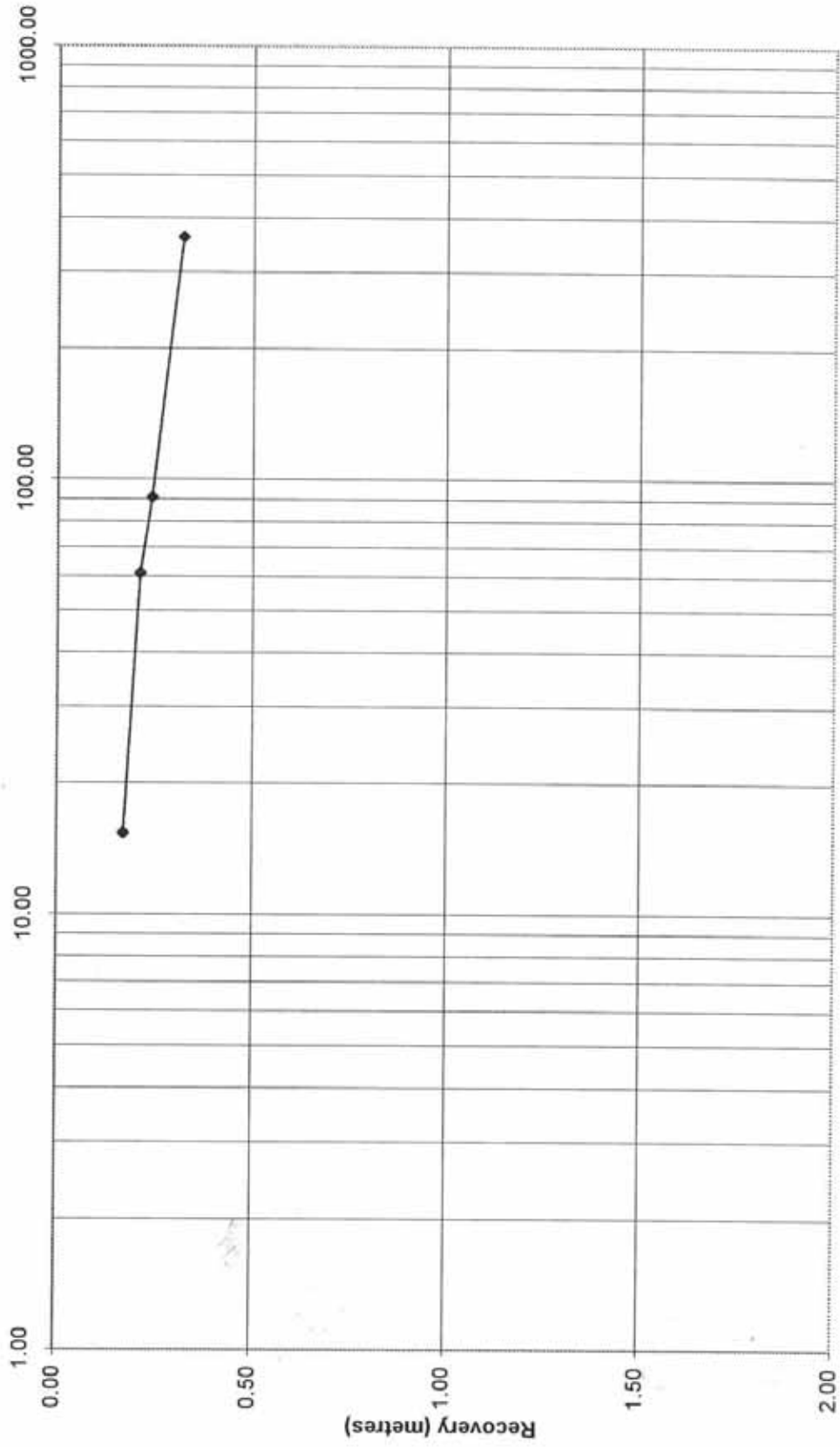
RECOVERY DATA

Proposed Residential Subdivision

TW1

RESIDUAL DRAWDOWN

t/t'



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APPENDIX E
PUMPING TEST DATA
TEST WELL 2

November 2004

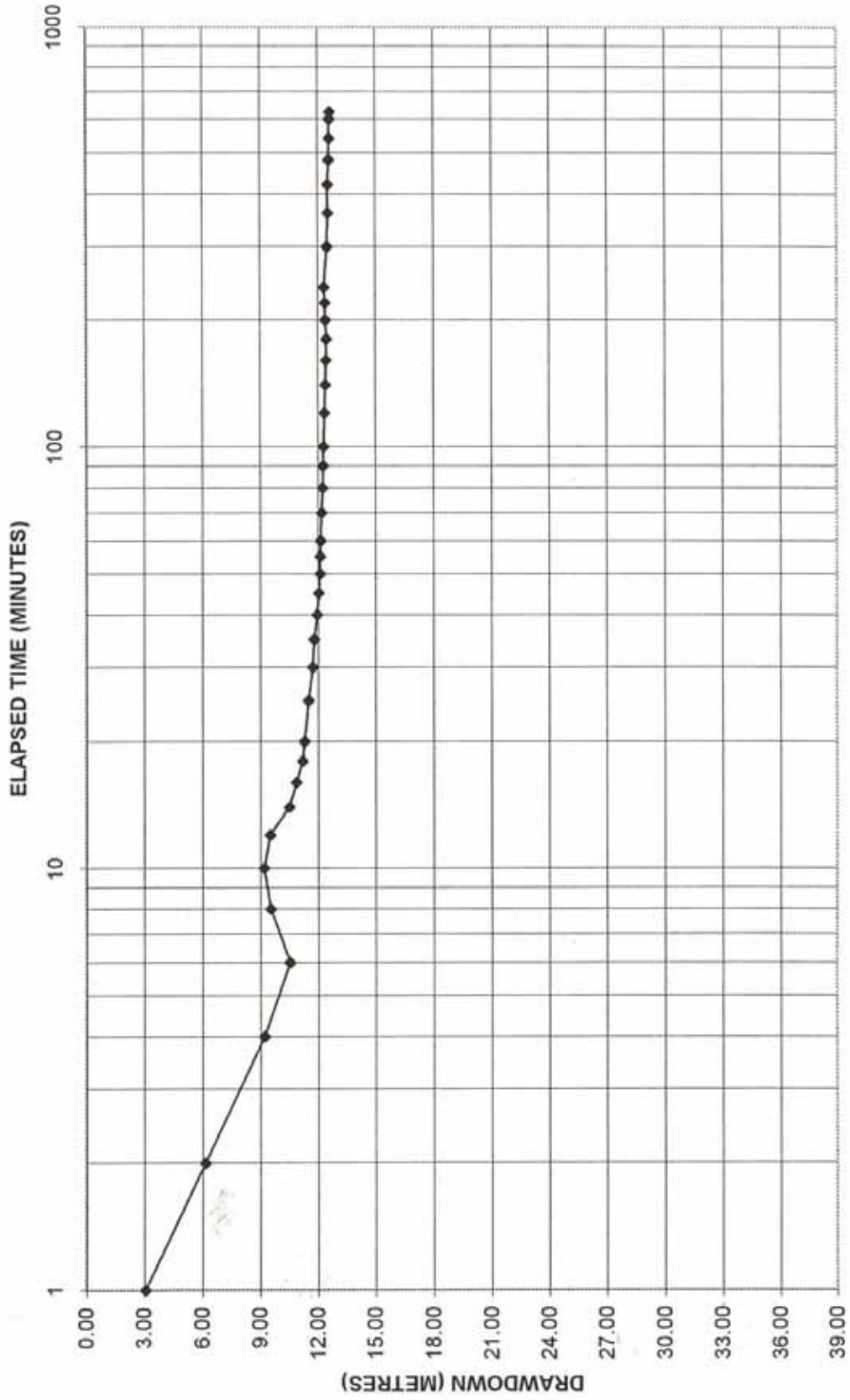
DRAWDOWN DATA
TW2
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of Casing (metres)	Drawdown (metres)
9:12:00	0:00:00	0	0.2	0.00
9:13:00	0:01:00	1	3.23	3.03
9:14:00	0:02:00	2	6.33	6.13
9:16:00	0:04:00	4	9.41	9.21
9:18:00	0:06:00	6	10.72	10.52
9:20:00	0:08:00	8	9.72	9.52
9:22:00	0:10:00	10	9.37	9.17
9:24:00	0:12:00	12	9.69	9.49
9:26:00	0:14:00	14	10.71	10.51
9:28:00	0:16:00	16	11.07	10.87
9:30:00	0:18:00	18	11.39	11.19
9:32:00	0:20:00	20	11.48	11.28
9:37:00	0:25:00	25	11.71	11.51
9:42:00	0:30:00	30	11.92	11.72
9:47:00	0:35:00	35	11.99	11.79
9:52:00	0:40:00	40	12.16	11.96
9:57:00	0:45:00	45	12.24	12.04
10:02:00	0:50:00	50	12.30	12.10
10:07:00	0:55:00	55	12.32	12.12
10:12:00	1:00:00	60	12.34	12.14
10:22:00	1:10:00	70	12.39	12.19
10:32:00	1:20:00	80	12.43	12.23
10:42:00	1:30:00	90	12.46	12.26
10:52:00	1:40:00	100	12.50	12.30
11:12:00	2:00:00	120	12.54	12.34
11:32:00	2:20:00	140	12.59	12.39
11:52:00	2:40:00	160	12.63	12.43
12:12:00	3:00:00	180	12.65	12.45
12:32:00	3:20:00	200	12.61	12.41
12:52:00	3:40:00	220	12.58	12.38
13:12:00	4:00:00	240	12.52	12.32
14:12:00	5:00:00	300	12.67	12.47
15:12:00	6:00:00	360	12.72	12.52
16:12:00	7:00:00	420	12.74	12.54
17:12:00	8:00:00	480	12.78	12.58
18:12:00	9:00:00	540	12.80	12.60
19:12:00	10:00:00	600	12.82	12.62
19:37:00	10:25:00	625	12.83	12.63

Proposed Residential Subdivision

TW2

DRAWDOWN VERSUS LOGTIME



RECOVERY DATA
TW2
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
19:40:00	0:00:00	0	360	0.00	12.83	12.63
19:41:00	0:01:00	1	361	361.00	9.75	9.55
19:42:00	0:02:00	2	362	181.00	7.14	6.94
19:44:00	0:04:00	4	364	91.00	2.07	1.87
19:46:00	0:06:00	6	366	61.00	0.73	0.53
19:48:00	0:08:00	8	368	46.00	0.39	0.19
19:58:00	0:18:00	18	378	21.00	0.34	0.14

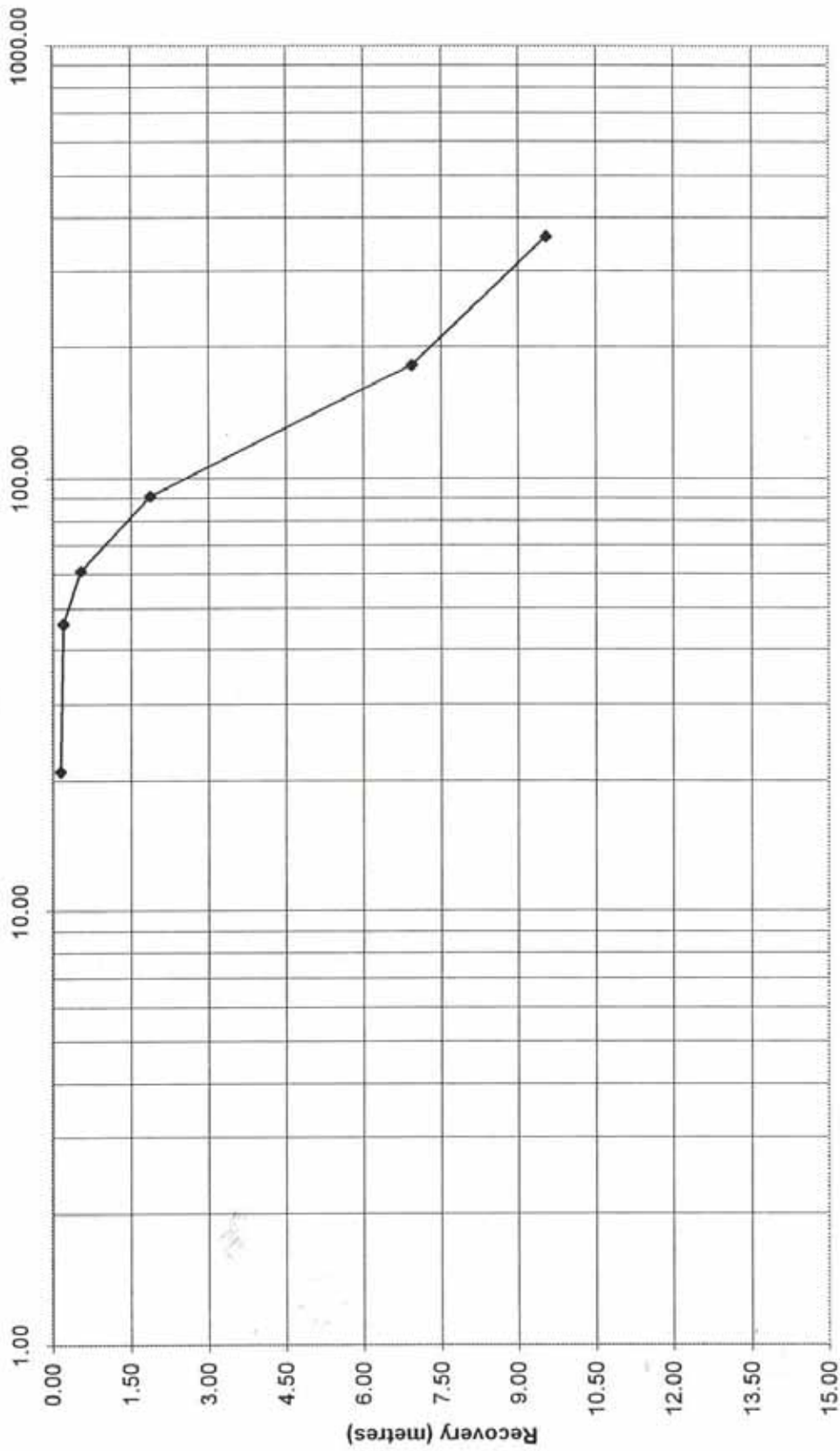
RECOVERY DATA

Proposed Residential Subdivision

TW2

RESIDUAL DRAWDOWN

t/t'



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APPENDIX F
PUMPING TEST DATA
TEST WELL 3

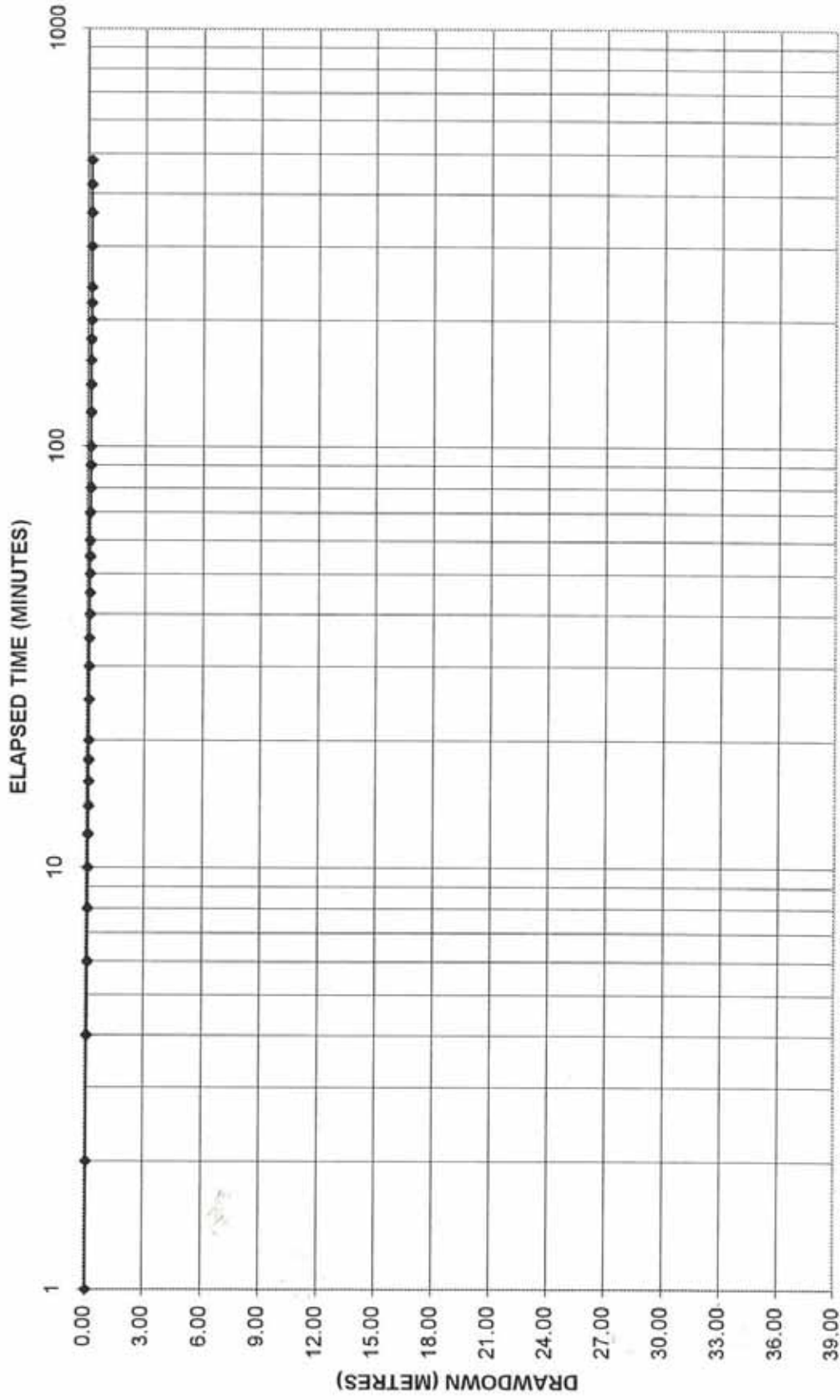
DRAWDOWN DATA
 TW3
 Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of	
			Casing (metres)	Drawdown (metres)
8:42:00	0:00:00	0	2.65	0.00
8:43:00	0:01:00	1	2.71	0.06
8:44:00	0:02:00	2	2.71	0.06
8:46:00	0:04:00	4	2.71	0.06
8:48:00	0:06:00	6	2.72	0.07
8:50:00	0:08:00	8	2.73	0.08
8:52:00	0:10:00	10	2.73	0.08
8:54:00	0:12:00	12	2.74	0.09
8:56:00	0:14:00	14	2.75	0.10
8:58:00	0:16:00	16	2.75	0.10
9:00:00	0:18:00	18	2.75	0.10
9:02:00	0:20:00	20	2.75	0.10
9:07:00	0:25:00	25	2.75	0.10
9:12:00	0:30:00	30	2.76	0.11
9:17:00	0:35:00	35	2.76	0.11
9:22:00	0:40:00	40	2.77	0.12
9:27:00	0:45:00	45	2.78	0.13
9:32:00	0:50:00	50	2.78	0.13
9:37:00	0:55:00	55	2.78	0.13
9:42:00	1:00:00	60	2.79	0.14
9:52:00	1:10:00	70	2.79	0.14
10:02:00	1:20:00	80	2.80	0.15
10:12:00	1:30:00	90	2.80	0.15
10:22:00	1:40:00	100	2.81	0.16
10:42:00	2:00:00	120	2.82	0.17
11:02:00	2:20:00	140	2.82	0.17
11:22:00	2:40:00	160	2.82	0.17
11:42:00	3:00:00	180	2.82	0.17
12:02:00	3:20:00	200	2.83	0.18
12:22:00	3:40:00	220	2.83	0.18
12:42:00	4:00:00	240	2.83	0.18
13:42:00	5:00:00	300	2.83	0.18
14:42:00	6:00:00	360	2.83	0.18
15:42:00	7:00:00	420	2.83	0.18
16:02:00	8:00:00	480	2.83	0.18

Proposed Residential Subdivision

TW3

DRAWDOWN VERSUS LOGTIME



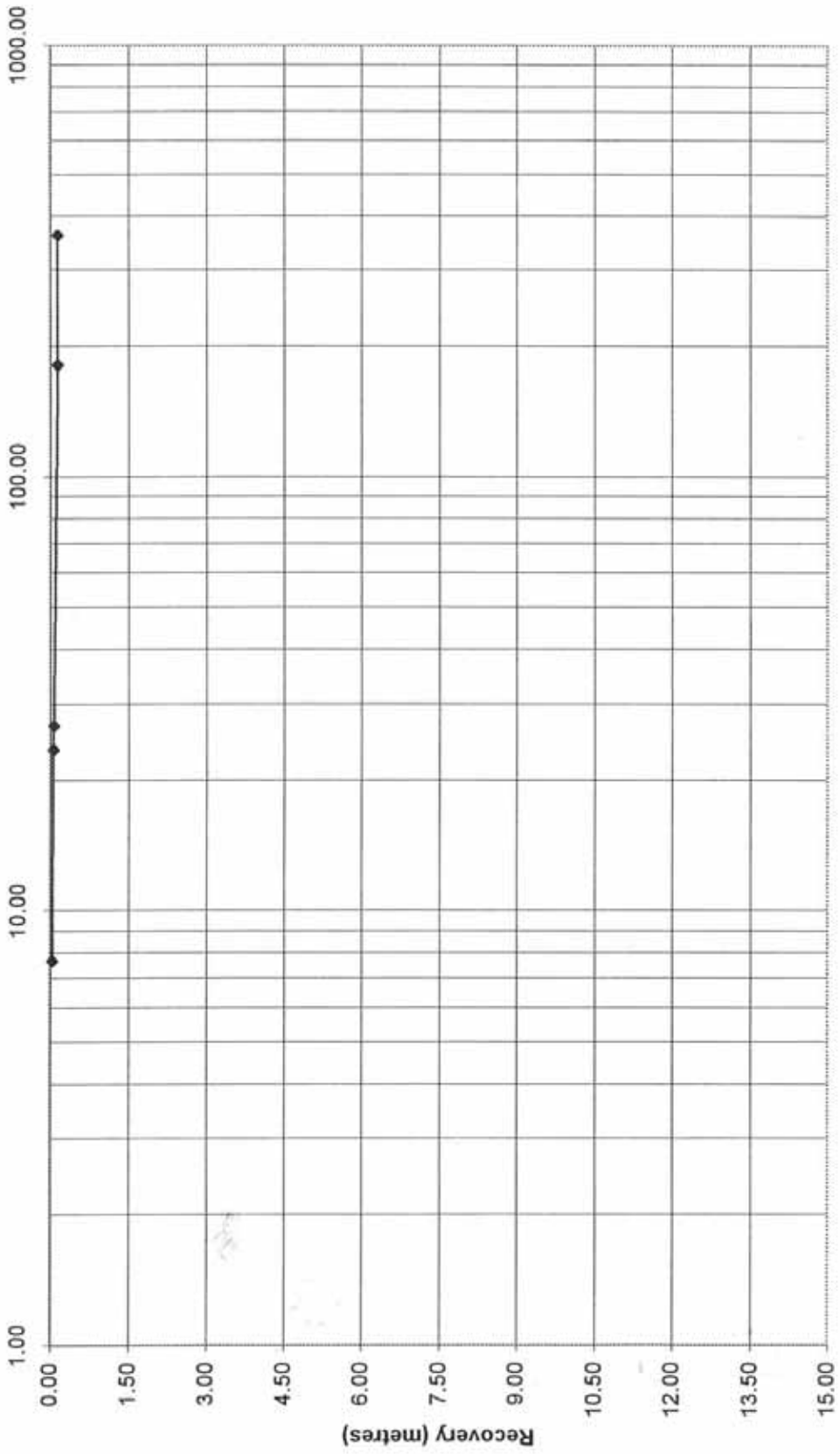
RECOVERY DATA
TW3
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
16:02:00	0:00:00	0	360	0.00	2.83	0.18
16:03:00	0:01:00	1	361	361.00	2.78	0.13
16:04:00	0:02:00	2	362	181.00	2.78	0.13
16:16:00	0:04:00	14	374	26.71	2.71	0.06
16:18:00	0:06:00	16	376	23.50	2.70	0.05
16:56:00	0:08:00	54	414	7.67	2.68	0.03

RECOVERY DATA

Proposed Residential Subdivision
TW3

RESIDUAL DRAWDOWN
t/t'



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APPENDIX G
PUMPING TEST DATA
TEST WELL 4

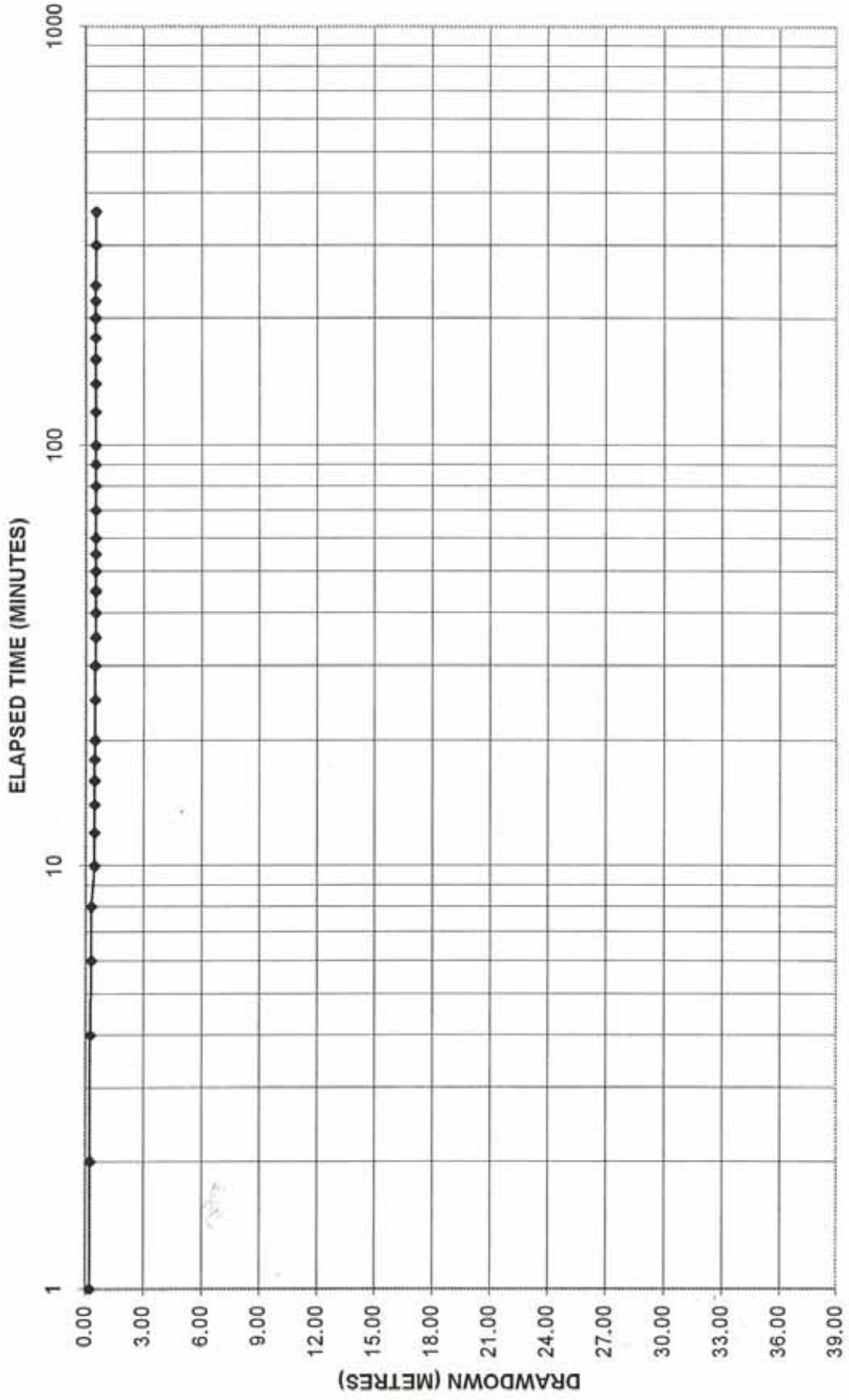
DRAWDOWN DATA
 TW4
 Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of	
			Casing (metres)	Drawdown (metres)
10:05:00	0:00:00	0	5.19	0.00
10:06:00	0:01:00	1	5.41	0.22
10:07:00	0:02:00	2	5.42	0.23
10:09:00	0:04:00	4	5.43	0.24
10:11:00	0:06:00	6	5.49	0.30
10:13:00	0:08:00	8	5.49	0.30
10:15:00	0:10:00	10	5.64	0.45
10:17:00	0:12:00	12	5.64	0.45
10:19:00	0:14:00	14	5.65	0.46
10:21:00	0:16:00	16	5.65	0.46
10:23:00	0:18:00	18	5.65	0.46
10:25:00	0:20:00	20	5.66	0.47
10:30:00	0:25:00	25	5.67	0.48
10:35:00	0:30:00	30	5.67	0.48
10:40:00	0:35:00	35	5.68	0.49
10:45:00	0:40:00	40	5.68	0.49
10:50:00	0:45:00	45	5.68	0.49
10:55:00	0:50:00	50	5.69	0.50
11:00:00	0:55:00	55	5.69	0.50
11:05:00	1:00:00	60	5.69	0.50
11:15:00	1:10:00	70	5.69	0.50
11:25:00	1:20:00	80	5.69	0.50
11:35:00	1:30:00	90	5.70	0.51
11:45:00	1:40:00	100	5.70	0.51
12:05:00	2:00:00	120	5.70	0.51
12:25:00	2:20:00	140	5.70	0.51
12:45:00	2:40:00	160	5.70	0.51
13:05:00	3:00:00	180	5.70	0.51
13:25:00	3:20:00	200	5.70	0.51
13:45:00	3:40:00	220	5.70	0.51
14:05:00	4:00:00	240	5.70	0.51
15:05:00	5:00:00	300	5.71	0.52
16:05:00	6:00:00	360	5.72	0.53

Proposed Residential Subdivision

TW4

DRAWDOWN VERSUS LOGTIME



RECOVERY DATA
TW4
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
16:05:00	0:00:00	0	360	0.00	5.72	0.53
16:06:00	0:01:00	1	361	361.00	5.34	0.15
16:07:00	0:02:00	2	362	181.00	5.34	0.15
16:25:00	0:20:00	20	380	19.00	5.29	0.10
16:35:00	0:30:00	30	390	13.00	5.25	0.06

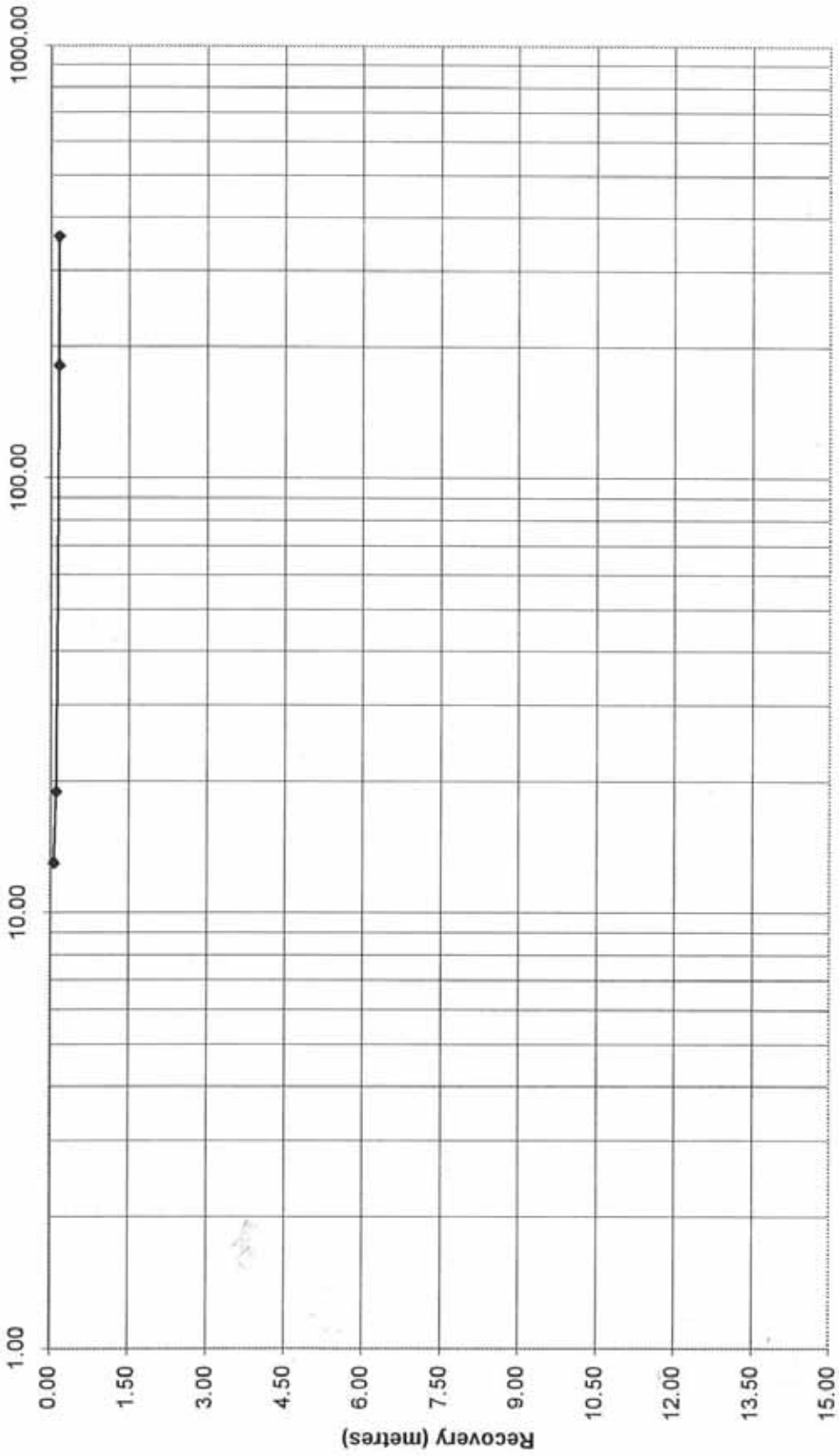
RECOVERY DATA

Proposed Residential Subdivision

TW4

RESIDUAL DRAWDOWN

t/t'



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APPENDIX H
PUMPING TEST DATA
TEST WELL 5

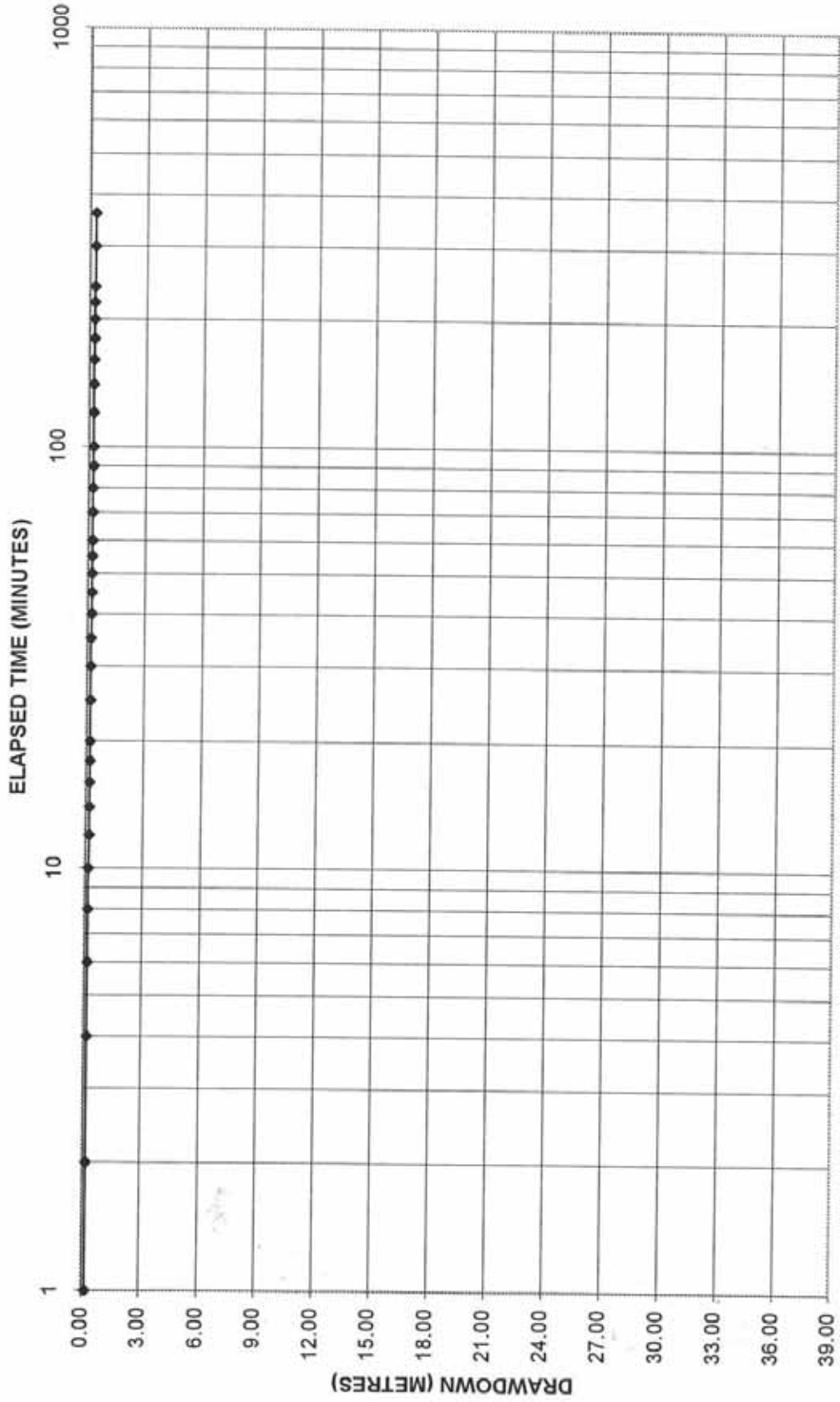
DRAWDOWN DATA
TW5
Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of	
			Casing (metres)	Drawdown (metres)
12:25:00	0:00:00	0	4.45	0.00
12:26:00	0:01:00	1	4.60	0.15
12:27:00	0:02:00	2	4.61	0.16
12:29:00	0:04:00	4	4.62	0.17
12:31:00	0:06:00	6	4.62	0.17
12:33:00	0:08:00	8	4.62	0.17
12:35:00	0:10:00	10	4.62	0.17
12:37:00	0:12:00	12	4.63	0.18
12:39:00	0:14:00	14	4.63	0.18
12:41:00	0:16:00	16	4.63	0.18
12:43:00	0:18:00	18	4.64	0.19
12:45:00	0:20:00	20	4.64	0.19
12:50:00	0:25:00	25	4.64	0.19
12:55:00	0:30:00	30	4.64	0.19
13:00:00	0:35:00	35	4.64	0.19
13:05:00	0:40:00	40	4.65	0.20
13:10:00	0:45:00	45	4.65	0.20
13:15:00	0:50:00	50	4.65	0.20
13:20:00	0:55:00	55	4.66	0.21
13:25:00	1:00:00	60	4.66	0.21
13:35:00	1:10:00	70	4.67	0.22
13:45:00	1:20:00	80	4.67	0.22
13:55:00	1:30:00	90	4.68	0.23
14:05:00	1:40:00	100	4.68	0.23
14:25:00	2:00:00	120	4.68	0.23
14:45:00	2:20:00	140	4.69	0.24
15:05:00	2:40:00	160	4.69	0.24
15:25:00	3:00:00	180	4.71	0.26
15:45:00	3:20:00	200	4.71	0.26
16:05:00	3:40:00	220	4.71	0.26
16:25:00	4:00:00	240	4.72	0.27
17:25:00	5:00:00	300	4.73	0.28
18:25:00	6:00:00	360	4.73	0.28

Proposed Residential Subdivision

TW5

DRAWDOWN VERSUS LOGTIME



RECOVERY DATA
 TW5
 Proposed Residential Subdivision

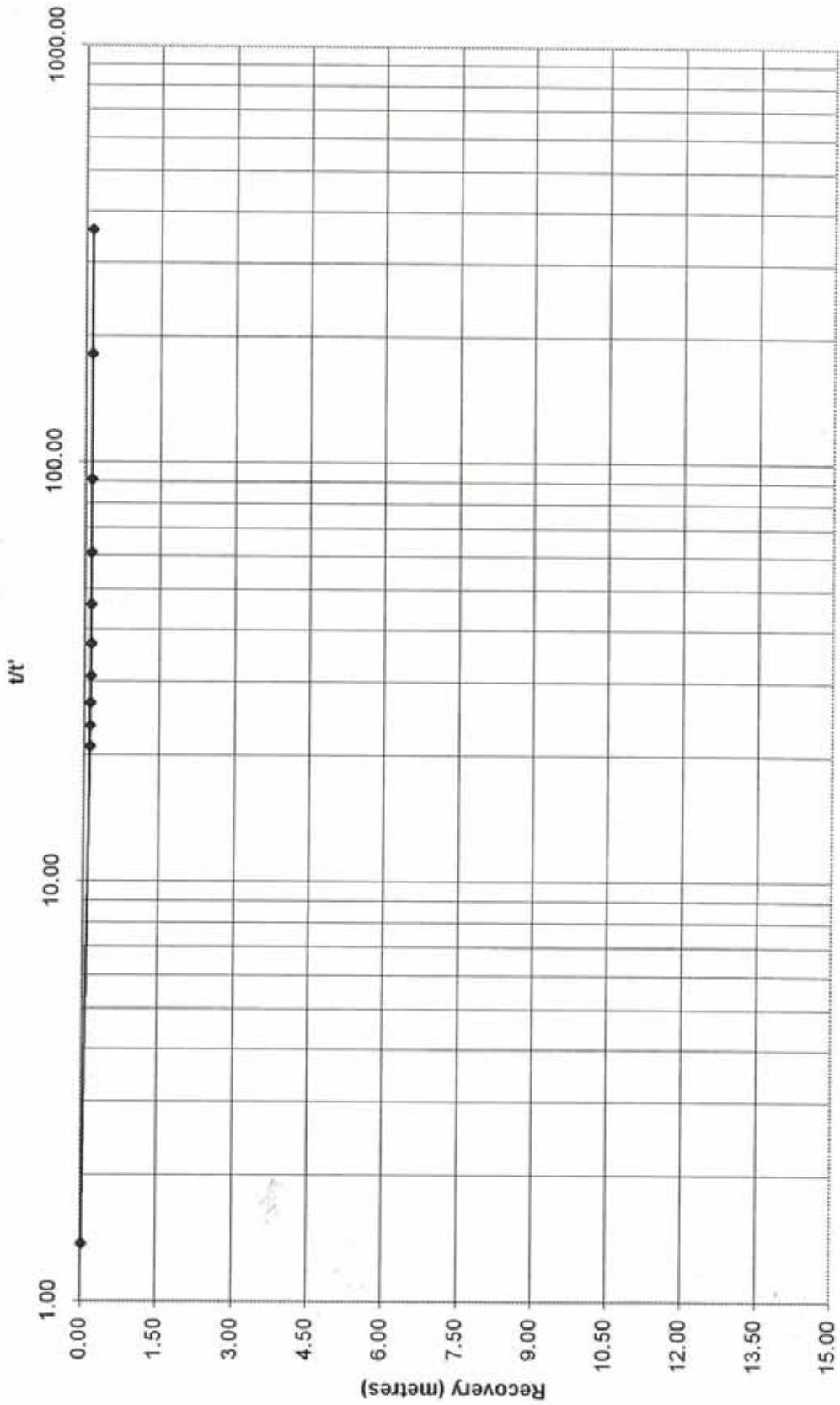
Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
18:25:00	0:00:00	0	360	0.00	4.73	0.28
18:26:00	0:01:00	1	361	361.00	4.57	0.12
18:27:00	0:02:00	2	362	181.00	4.57	0.12
18:29:00	0:04:00	4	364	91.00	4.57	0.12
18:31:00	0:06:00	6	366	61.00	4.57	0.12
18:33:00	0:08:00	8	368	46.00	4.57	0.12
18:35:00	0:10:00	10	370	37.00	4.57	0.12
18:37:00	0:12:00	12	372	31.00	4.57	0.12
18:39:00	0:14:00	14	374	26.71	4.56	0.11
18:41:00	0:16:00	16	376	23.50	4.56	0.11
18:43:00	0:18:00	18	378	21.00	4.56	0.11
10:30:00	16:05:00	965	1325	1.37	4.46	0.01

RECOVERY DATA

Proposed Residential Subdivision

TW5

RESIDUAL DRAWDOWN



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APPENDIX I
PUMPING TEST DATA
TEST WELL 6

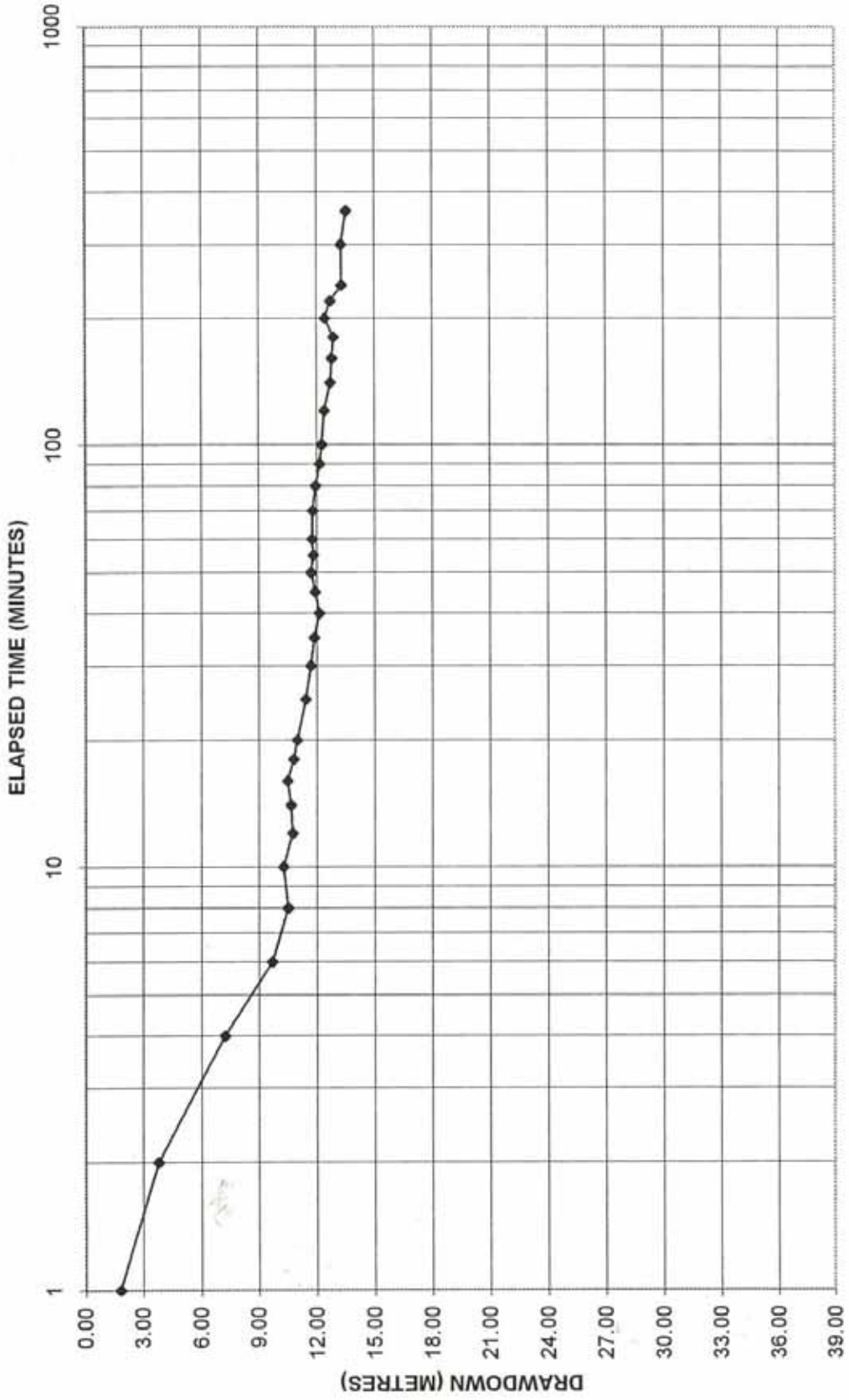
DRAWDOWN DATA
 TW6
 Proposed Residential Subdivision

Time	Elapsed Time (hours)	Elapsed Time (min)	Water Level Below Top of	
			Casing (metres)	Drawdown (metres)
10:55:00	0:00:00	0	5.93	0.00
10:56:00	0:01:00	1	7.72	1.79
10:57:00	0:02:00	2	9.72	3.79
10:59:00	0:04:00	4	13.15	7.22
11:01:00	0:06:00	6	15.61	9.68
11:03:00	0:08:00	8	16.43	10.50
11:05:00	0:10:00	10	16.20	10.27
11:07:00	0:12:00	12	16.67	10.74
11:09:00	0:14:00	14	16.58	10.65
11:11:00	0:16:00	16	16.41	10.48
11:13:00	0:18:00	18	16.71	10.78
11:15:00	0:20:00	20	16.89	10.96
11:20:00	0:25:00	25	17.35	11.42
11:25:00	0:30:00	30	17.62	11.69
11:30:00	0:35:00	35	17.80	11.87
11:35:00	0:40:00	40	18.06	12.13
11:40:00	0:45:00	45	17.86	11.93
11:45:00	0:50:00	50	17.65	11.72
11:50:00	0:55:00	55	17.74	11.81
11:55:00	1:00:00	60	17.69	11.76
12:05:00	1:10:00	70	17.71	11.78
12:15:00	1:20:00	80	17.88	11.95
12:25:00	1:30:00	90	18.08	12.15
12:35:00	1:40:00	100	18.20	12.27
12:55:00	2:00:00	120	18.34	12.41
13:15:00	2:20:00	140	18.65	12.72
13:35:00	2:40:00	160	18.73	12.80
13:55:00	3:00:00	180	18.81	12.88
14:15:00	3:20:00	200	18.36	12.43
14:35:00	3:40:00	220	18.65	12.72
14:55:00	4:00:00	240	19.24	13.31
15:55:00	5:00:00	300	19.20	13.27
16:55:00	6:00:00	360	19.46	13.53

Proposed Residential Subdivision

TW6

DRAWDOWN VERSUS LOGTIME



RECOVERY DATA
TW6
Proposed Residential Subdivision

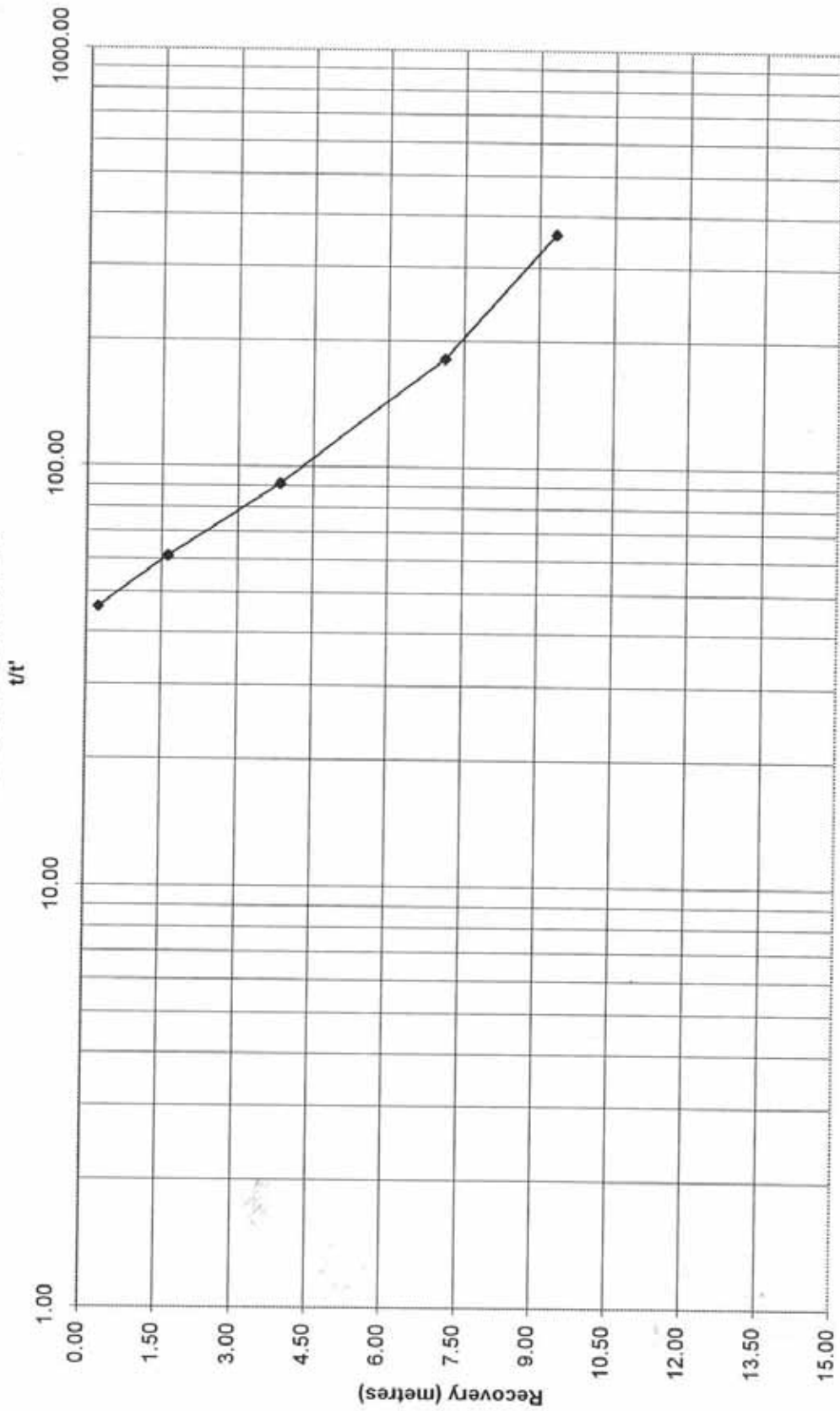
Time	Elapsed Time (hours)	Elapsed Time (min) t'	Time Since Pump Test Started (min) t	Ratio t/t'	Water Level Below Top of Casing (metres)	Recovery (metres)
16:55:00	0:00:00	0	360	0.00	19.46	13.53
16:56:00	0:01:00	1	361	361.00	15.27	9.34
16:57:00	0:02:00	2	362	181.00	13.06	7.13
16:59:00	0:04:00	4	364	91.00	9.77	3.84
17:01:00	0:06:00	6	366	61.00	7.55	1.62
17:03:00	0:08:00	8	368	46.00	6.17	0.24

RECOVERY DATA

Proposed Residential Subdivision

TW6

RESIDUAL DRAWDOWN



February 2005

041-444

APPENDIX J
SEPTIC EFFLUENT DILUTION CALCULATIONS

 SEPTIC EFFLUENT DILUTION CALCULATIONS

The lesser of MOE water surplus for Ottawa sandy soils
/Merrickville water surplus area

364 millimetres

Site area – hard surfaces (conservatively 20 percent)

$980,000 \times 0.8 = 784,000$

Infiltration Reduction Factor (IRF)

Topography (Flat Land)

0.3

Soil (Sand)

0.4

Cover (Woodland)

0.2

Total

0.9

Background Nitrate Level

1.27 mg/l

Dilution Calculation for 67 Proposed Septic Systems:

$$1.27 \text{ mg/l} + \frac{67 \times 365 \text{ m}^3 \text{ effluent per year} \times 40 \text{ mg/l NO}_3}{67 \times 365 \text{ m}^3 \text{ effluent} + (784,000 \text{ m}^2 \times 0.364 \text{ m NPI} \times 0.9 \text{ IRF})} = 4.7 \text{ mg/l NO}_3$$

February 2005

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APPENDIX K

RESULTS OF LABORATORY NITRATE TESTING
OF MONITORING WELL WATER SAMPLES

ACCU TEST LABORATORIES LTD

REPORT OF ANALYSIS

Client: Morey Houle Chevrolet Engineering
 28 Clegher St. E., Unit B, Box 910
 Kemptville, ON
 K0G 1J0

Report Number: 2502059
 Date: 2005-02-28
 Date Submitted: 2005-02-23

Attention: Mr. Randy Morey

Project: 041-444

P.O. Number:

Matrix: Water

PARAMETER	UNITS	MDL	LAB ID:				TYPE	LIMIT	UNITS
			370494	370495	370496	370497			
Alkalinity as CaCO3	mg/L	5	265						
Chloride	mg/L	1	8						
Colour	TCU	2	<2						
Conductivity	uS/cm	5	521						
Dissolved Organic Carbon	mg/L	0.5	0.7						
Fluoride	mg/L	0.10	0.17						
Hydrogen Sulphide	mg/L	0.01	<0.01						
N-NH3 (Ammonia)	mg/L	0.02	0.02						
N-NO2 (Nitrite)	mg/L	0.10	<0.10						
N-NO3 (Nitrate)	mg/L	0.10	0.23	1.27	0.56	<0.10	<0.10		
pH			7.55						
Phenols	mg/L	0.001	<0.001						
Sulphate	mg/L	1	24						
Tannin & Lignin	mg/L	0.1	<0.1						
TDS (COND - CALC)	mg/L	5	339						
Total Kjeldahl Nitrogen	mg/L	0.05	0.05						
Turbidity	NTU	0.1	0.3						
Hardness as CaCO3	mg/L	1	278						
Ion Balance		0.01	0.96						
Calcium	mg/L	1	70						
Magnesium	mg/L	1	25						
Potassium	mg/L	1	2						
Sodium	mg/L	2	4						
Iron	mg/L	0.01	0.01						
Manganese	mg/L	0.01	<0.01						

MDL = Method Detection Limit INC = Incomplete AO = Aesthetic Objective OG = Operational Guideline MAC = Maximum Allowable Concentration IAC = Interim Maximum Allowable Concentration

Comment:

APPROVAL

Ewan McRobbie
 ANALYST